



Lecture 13

4. Beam optics in circular accelerators

4.4 FODO cell

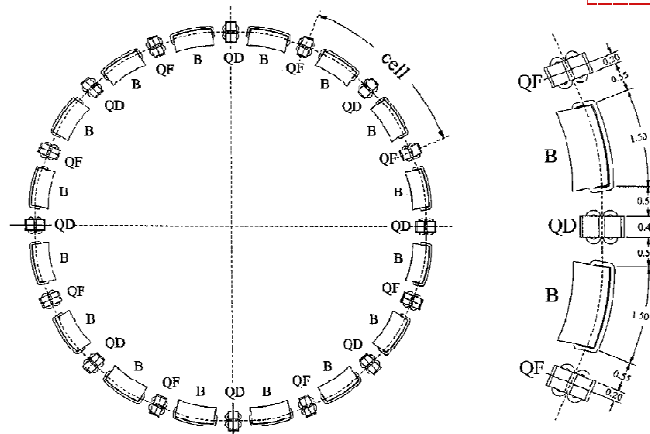
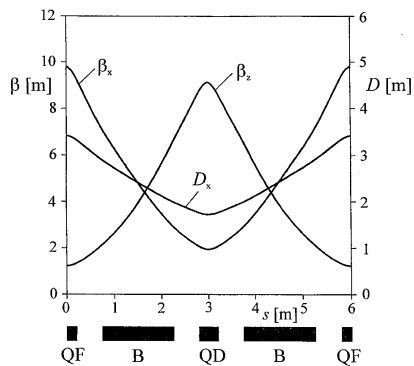
4.5 The periodic (closed) orbit

4.6 Closed orbit for $\Delta p \neq 0$



4.4 The FODO cell

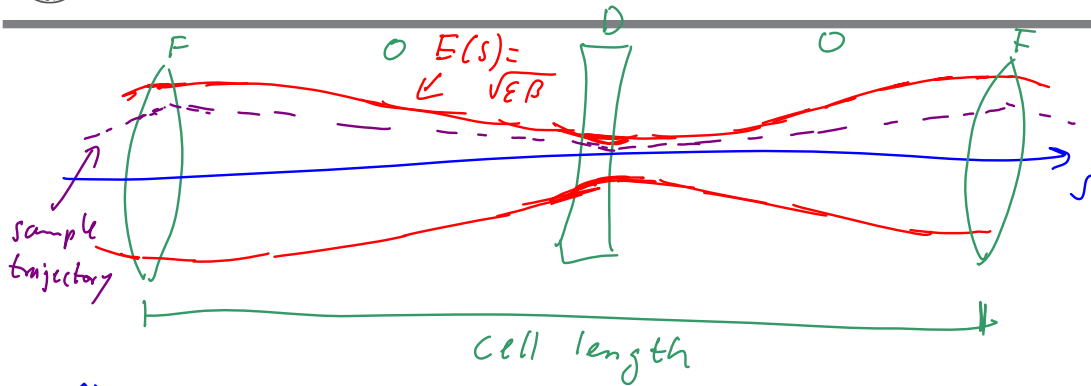
Alternating gradients allow focusing in both transverse planes. Therefore focusing and defocusing quadrupoles are usually alternated and interleaved with bending magnets.



The periodic beta function and dispersion for each FODO is also periodic for an accelerator section that consists of many FODO cells. Often large sections of an accelerator consist of FODOs.



Example: Thin lens FODO cell



\rightarrow in "thin lens" approximation with drift between quadrupoles:
 \Rightarrow for horizontal planes: thin lens: $\left| \frac{1}{f} \right| = ke$

$$M_{FODO} = Q\left(-\frac{ke}{2}\right) D\left(\frac{L}{2}\right) Q\left(\frac{ke}{2}\right) Q\left(\frac{ke}{2}\right) D\left(\frac{L}{2}\right) Q\left(-\frac{ke}{2}\right)$$



$$\begin{aligned}
 \Rightarrow M_{FODO} &= \begin{pmatrix} 1 & 0 \\ -\frac{ke}{2} & 1 \end{pmatrix} \begin{pmatrix} 1 & L/2 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ \frac{ke}{2} & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ \frac{ke}{2} & 1 \end{pmatrix} \begin{pmatrix} 1 & L/2 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ -\frac{ke}{2} & 1 \end{pmatrix} \\
 &= \begin{pmatrix} 1 + \frac{ke}{2} \frac{L}{2} & \frac{L}{2} \\ -\left(\frac{ke}{2}\right)^2 \frac{L}{2} & 1 - \frac{ke}{2} \frac{L}{2} \end{pmatrix} \begin{pmatrix} 1 - \frac{ke}{2} \frac{L}{2} & \frac{L}{2} \\ -\left(\frac{ke}{2}\right)^2 \frac{L}{2} & 1 + \frac{ke}{2} \frac{L}{2} \end{pmatrix} \\
 &= \begin{pmatrix} 1 - 2\xi^2 & L(1+\xi) \\ -\left(\frac{ke}{2}\right)^2 L(1-\xi) & 1 - 2\xi^2 \end{pmatrix} \quad \text{with } \xi \equiv \frac{ke}{2} \frac{L}{2}
 \end{aligned}$$



$$\Rightarrow \textcircled{1} \quad \cos \mu = \frac{1}{2} \text{ trace } \underline{M}_{\text{FODO}} = 1 - 2\xi^2$$

$$\Rightarrow \text{with } \cos \mu = 1 - 2 \sin^2 \mu/2$$

$$\Rightarrow \boxed{\left| \sin\left(\frac{\mu}{2}\right) \right| = |\xi|} \quad \text{for FODO cell}$$

$$\Rightarrow \text{stability requires: } |\text{trace } \underline{M}_{\text{FODO}}| < 2$$

$$\Rightarrow \text{need } \xi < 1 \Rightarrow \frac{kl}{2} \frac{L}{2} < 1$$

$$\Rightarrow \text{need focal length } \boxed{f = \frac{1}{kl} > \frac{L}{4}}$$

\Rightarrow gives upper limit for focal strength
with betatron phase advance per FODO cell: $0^\circ < \mu < 180^\circ$



$\textcircled{2}$ β -function at FODO cell entrance/exit:
(at center of focusing quad)

$$\hat{\beta}_x = M_{\text{FODO},12} \frac{1}{\sin \mu} = \frac{L(1+\xi)}{\sin \mu}$$

$$\Rightarrow \boxed{\hat{\beta}_x = L \frac{1 + \sin(\mu/2)}{\sin \mu}}$$

$\textcircled{3}$ α -function at FODO cell entrance/exit:
(at center of focusing quad)

$$\alpha = (M_{\text{FODO},11} - M_{\text{FODO},22}) \frac{1}{2 \sin \mu} = 0$$

\Rightarrow expected from symmetry



④ β -function at FODO cell center (center of defocusing quadrupole):

$$\text{use } \check{\beta} = C^2 \hat{\beta} + S^2 \frac{1}{\hat{\beta}} \quad \text{since } \alpha_0 = 0$$

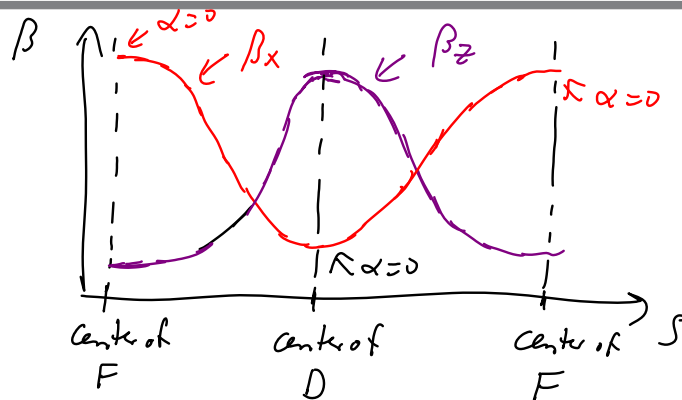
↑ from transport matrix of first half

of FODO cell: $Q(\frac{\mu L}{2}) D(\frac{L}{2}) Q(-\frac{\mu L}{2})$

$$\text{have } C_{1/2 \text{ FODO}} = 1 - \mathcal{F} \quad S_{1/2 \text{ FODO}} = L/2$$

$$\Rightarrow \check{\beta} = (1 - \mathcal{F}) \hat{\beta} + \frac{L^2}{4} \frac{1}{\hat{\beta}}$$

$$\Rightarrow \boxed{\check{\beta}_x = L \frac{1 - \sin \mu/2}{\sin \mu}}$$





4.5 The periodic (closed) orbit

so far: design orbit of circular machine

→ closed curve ⇒ periodic

$\vec{u}(s) = 0$ { → particle with $u_0 = 0$, $u_0' = 0$, $\delta = 0$
travels on design orbit

$\vec{u}_p(s) = \underline{M} \vec{u}_p(0)$ { → particles with $u_0 \neq 0$ and/or $u_0' \neq 0$,
but $\delta = 0$ will conduct betatron oscillations
about design orbit

Note: path of particles around ring
does not close onto itself
since the ν -value is non-
integer!



now: consider distorted orbit:

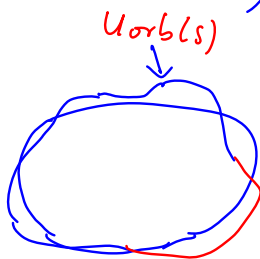
→ eg. from extra kick from dipole field error,
particle with momentum error (i.e. $\delta \neq 0$)

...

⇒ The design orbit is no longer a
possible trajectory for a particle!

⇒ new, distorted closed orbit

note: for stable beam operation,
this must be still a
periodic, closed orbit!



$$\vec{u} = \vec{u}_{orb}(s)$$

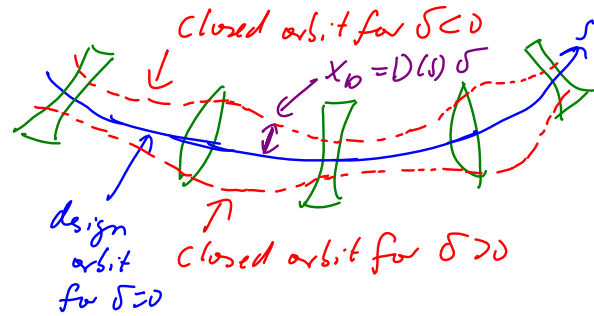
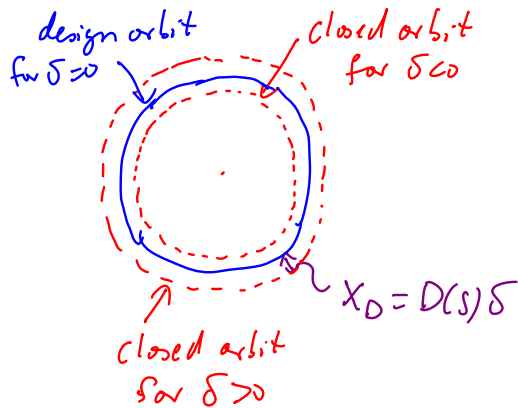
$$\text{with } \vec{u}_{orb}(s+L) = \vec{u}_{orb}(s)$$



=> Example: Particle with momentum error.

weakly focusing
circular accelerator

strongly focusing circular
accelerator



=> closed dispersion orbit defined by

$$x_D(s) = \underbrace{D(s)}_{\text{closed, periodic dispersion function}} \delta$$

closed, periodic
dispersion function

$$D(s+L) = D(s)$$

$$D'(s+L) = D'(s)$$

=> particles with $u_p(0) = 0$ and $u'_p(0) = 0$

move on closed distorted orbit

i.e. $\vec{u}(s) = \vec{u}^{\text{orbit}}(s)$



\Rightarrow particles with $u_p(0) \neq 0$ and/or $u_p'(0) \neq 0$ perform betatron oscillations about the distorted closed orbit, and not around the original design orbit!

$$\Rightarrow \vec{u}(s) = \underbrace{\vec{u}_{\text{orbit}}(s)} + \underbrace{\vec{u}_p(s)}$$

particular,
periodic solution
of the inhomog.
equ. of motion

solution of
the homogeneous
equ. of motion

$$\vec{u}_p(s) = \underline{M} \vec{u}_p(0)$$

as before!



equ. of motion: $u'' + \mathcal{K}(s)u = p(s)$

\uparrow
perturbation term
from magnetic field
error, particle error, ...

\Rightarrow $u_{\text{orb}}(s)$ is a periodic solution of this inhomogeneous equation of motion, i.e. need to find solution with $\vec{u}_{\text{orb}}(s+L) = \vec{u}_{\text{orb}}(s)$

\leadsto start with general solution (from before)

$$u(s) = a G'(s) + b S(s) + P(s)$$

with special (non-periodic!) solution of the inhomog. equation:



$$P(s) = S'(s) \int_0^s p(\tilde{s}) G'(s, \tilde{s}) d\tilde{s} - G'(s) \int_0^s p(\tilde{s}) S'(s, \tilde{s}) d\tilde{s}$$

~) need to find constants a and b to find periodic solution u_{arb} :

$$\begin{aligned} \text{at } s_0=0: \quad G'(s_0) &= 1 & G'(s_0) &= 0 \\ S'(s_0) &= 0 & S'(s_0) &= 1 \\ P(s_0) &= 0 & P'(s_0) &= 0 \end{aligned}$$

$$\text{need } u_{\text{arb}}(s_0) = u_{\text{arb}}(s_0 + L)$$

$$\text{gives: } a + 0 + 0 = aG'(L) + bS'(L) + P(L) \quad \textcircled{1}$$



$$\text{also need: } u_{\text{arb}}(0) = u_{\text{arb}}(L)$$

$$\text{gives: } 0 + b + 0 = aG'(L) + bS'(L) + P'(L) \quad \textcircled{2}$$

=> solve $\textcircled{2}$ for b , insert into $\textcircled{1}$

$$\Rightarrow a \left(1 - G'(L) - \frac{S'(L)G'(L)}{1 - S'(L)} \right) = \frac{S(L)P'(L)}{1 - S'(L)} + P(L)$$

$$\Rightarrow a = \frac{S(L)P'(L) - \{S'(L) - 1\}P(L)}{\{G'(L) - 1\}\{S'(L) - 1\} - S(L)G'(L)}$$



~) The denominator is:

$$\text{denom} = 1 + \underbrace{\{C'(L)S'(L) - S(L)C'(L)\}}_{\det M = 1} - \underbrace{\{C'(L) + S'(L)\}}_{\text{trace } M = 2 \cos \mu}$$

$$= 2 - 2 \cos \mu = 4 \sin^2(\mu/2)$$

↑
betatron phase advance per full turn
= $2\pi \cdot \text{turns}$



~) The numerator is:

$$\begin{aligned} \text{num.} &= S(L) \left\{ S'(L) \int_0^L p(s) G'(s) ds - C'(L) \int_0^L p(s) S(s) ds \right\} \\ &\quad - (S'(L) - 1) \left\{ S(L) \int_0^L p(s) G'(s) ds - C(L) \int_0^L p(s) S(s) ds \right\} \\ &= \underbrace{\{C(L)S'(L) - S(L)C'(L)\}}_{\det M = 1} \int_0^L p S ds - C(L) \int_0^L p S ds \\ &\quad + S(L) \int_0^L p G' ds \end{aligned}$$



for periodic structure:

$$M(0 \rightarrow L) = \begin{pmatrix} \cos \mu + \alpha_0 \sin \mu & \beta_0 \sin \mu \\ -\gamma_0 \sin \mu & \cos \mu - \alpha_0 \sin \mu \end{pmatrix}$$

$$\Rightarrow G(L) = \cos \mu + \alpha_0 \sin \mu$$

$$S'(L) = \beta_0 \sin \mu$$

$$\Rightarrow \text{num.} = (1 - \cos \mu - \alpha_0 \sin \mu) \int_0^L p(\tilde{s}) S'(\tilde{s}) d\tilde{s} \\ + \beta_0 \sin \mu \int_0^L p(\tilde{s}) G(\tilde{s}) d\tilde{s}$$



\Rightarrow from general transport matrix in terms of
Twiss parameters:

$$G(s) = \sqrt{\beta/\beta_0} \left[\cos(\psi - \psi_0) + \alpha_0 \sin(\psi - \psi_0) \right]$$

$$S' = \sqrt{\beta\beta_0} \sin(\psi(s) - \psi_0)$$

$$\Rightarrow \text{num.} = (1 - \cos \mu - \alpha_0 \sin \mu) \int_0^L p(\tilde{s}) \sqrt{\beta(\tilde{s})} \sin(\psi(\tilde{s}) - \psi_0) d\tilde{s} \\ + \sqrt{\beta_0} \sin \mu \int_0^L p(\tilde{s}) \sqrt{\beta(\tilde{s})} \left[\cos(\psi(\tilde{s}) - \psi_0) + \alpha_0 \sin(\psi(\tilde{s}) - \psi_0) \right] d\tilde{s}$$

$$= \sqrt{\beta_0} 2 \sin\left(\frac{\mu}{2}\right) \int_0^L \sqrt{\beta(\tilde{s})} p(\tilde{s}) \cos\left\{\psi(\tilde{s}) - \psi_0 - \frac{\mu}{2}\right\} d\tilde{s}$$



now: $u_{\text{orb}}(0) = a$, point $s_0 = 0$ was
chosen arbitrarily!

$$\Rightarrow u_{\text{orb}}(s) = \frac{\sqrt{B(s)}}{2 \sin\left(\frac{\mu}{2}\right)} \int_{\text{full turn}} p(\tilde{s}) \sqrt{p(\tilde{s})} \omega \left\{ |\psi(\tilde{s}) - \psi(s)| - \frac{\mu}{2} \right\} d\tilde{s}$$

note: for $\mu = N 2\pi \Rightarrow$ instability!
(i.e. for tune $\nu = \text{integer}$)