177 **RF** in Accelerators $\vec{\nabla} \times \vec{E} = -\partial_t \vec{B} \qquad \left\{ \vec{\nabla} \times \left(\vec{\nabla} \times \vec{E} \right) = -\frac{1}{c^2} \partial_t^2 \vec{E} - \mu_0 \partial_t \vec{j} \\ \vec{\nabla} \times \vec{B} = \frac{1}{c^2} \partial_t \vec{E} + \mu_0 \vec{j} \right\} \quad \vec{\nabla} \times \left(\vec{\nabla} \times \vec{B} \right) = -\frac{1}{c^2} \partial_t^2 \vec{B} - \mu_0 \vec{\nabla} \times \vec{j}$ Wave guides: Wave equation for all components $\rho = ()$ $\vec{\nabla}^2 \vec{E} = \frac{1}{2} \partial_t^2 \vec{E}$ $\vec{i}=0$ $\vec{\nabla}^2 \vec{B} = \frac{1}{2} \partial_t^2 \vec{B}$ $\vec{\nabla} \times \vec{E} = -\partial_t \vec{B} \\ \vec{\nabla}_\perp \times \vec{E}_\perp = -\partial_t \vec{B}_z \\ \vec{\nabla}_\perp \times \vec{B} = \frac{1}{c^2} \partial_t \vec{E} \\ \vec{\nabla}_\perp \times \vec{B}_\perp = \frac{1}{c^2} \partial_t \vec{E}_z$ $\vec{\nabla} \cdot \vec{E} = 0 \left\{ \vec{\nabla}_{\perp} \cdot \vec{E}_{\perp} + \partial_{z}E_{z} = 0 \right\}$ $\vec{\nabla} \cdot \vec{B} = 0 \left\{ \vec{\nabla}_{\perp} \cdot \vec{B}_{\perp} + \partial_{z}B_{z} = 0 \right\}$ Search for simple modes: Transverse electric and magnetic (TEM) waves cannot exists, since: $E_z = 0$ and $B_z = 0 \implies \vec{E}_\perp = 0$ and $\vec{B}_\perp = 0$ Georg.Hoffstaetter@Cornell.edu 12-23 June 2006 **USPAS Advanced Accelerator Physics**





Dispersion relation



$$\omega(k_z) = c\sqrt{A_n^2 + k_z^2}$$

Phase velocity
$$v_{ph} = \omega / k_z = c \sqrt{1 + \left(\frac{A_n}{k_z}\right)^2} > c$$

Group velocity
$$v_{gr} = d\omega / dk_z = c / \sqrt{1 + \left(\frac{A_n}{k_z}\right)^2} < c$$

For each excitation frequency ω one obtains a propagation in the wave guide of

$$e^{ik_z z}$$
, $k_z = \sqrt{\left(\frac{\omega}{c}\right)^2 - A_n^2}$

Transport for ω above the cutoff frequency $\omega > \omega_n = cA_n$ Damping for ω below the cutoff frequency $\omega < \omega_n = cA_n$





Rectangular Wave Guide



Boundary conditions:

$$E_{z}(\vec{x}_{0}) = 0 \quad \vec{\nabla}_{\perp}^{2} E_{z} = [k_{z}^{2} - (\frac{\omega}{c})^{2}] E_{z}$$

$$E_{z}(\vec{x}) = E_{z} \sin(\frac{n\pi}{a} x) \sin(\frac{m\pi}{b} y)$$

$$(\frac{\omega}{c})^{2} - k_{z}^{2} = k_{nm}^{(B)2} = (\frac{n\pi}{a})^{2} + (\frac{m\pi}{b})^{2}$$

$$\partial_{r} B_{z}(\vec{x}_{0}) = 0 \quad \vec{\nabla}_{\perp}^{2} B_{z} = [k_{z}^{2} - (\frac{\omega}{c})^{2}] B_{z}$$

$$B_{z}(\vec{x}) = B_{z} \cos(\frac{n\pi}{a} x) \cos(\frac{m\pi}{b} y)$$

$$(\frac{\omega}{c})^{2} - k_{z}^{2} = k_{nm}^{(E)2} = (\frac{n\pi}{a})^{2} + (\frac{m\pi}{b})^{2}$$

TE and TM modes happen to have the same eigenvalues.

For simplicity one still looks at TE and TM modes separately.



Rectangular TE Modes



Boundary conditions:
$$E_z(\vec{x}) = 0$$

 $\vec{E}_{I/I}(\vec{x}_0) = 0$
 $E_x(\vec{x}) = [A\cos(\frac{n\pi}{a}x) + B\sin(\frac{n\pi}{a}x)]\sin(\frac{m\pi}{b}y)$
 $E_y(\vec{x}) = \sin(\frac{n\pi}{a}x)[C\cos(\frac{m\pi}{b}y) + D\sin(\frac{m\pi}{b}y)]$
 $\vec{\nabla}_{\perp} \cdot \vec{E}_{\perp} = 0 \implies D = 0, \quad B = 0, \quad C = -A\frac{n}{a}\frac{b}{m}$
 $\vec{\nabla}_{\perp} \cdot \vec{E}_{\perp} = i\omega B_z \cos(\frac{n\pi}{a}x)\cos(\frac{m\pi}{b}y) \implies A\frac{b}{m\pi}[(\frac{(m\pi)^2}{b})^2 + (\frac{n\pi}{a})^2] = -i\omega B_z$
 $\vec{B}_r(\vec{x}_0) = 0 \quad B_x(\vec{x}) = \sin(\frac{n\pi}{a}x)[C'\cos(\frac{m\pi}{b}y) + D'\sin(\frac{m\pi}{b}y)]$
 $B_y(\vec{x}) = [A'\cos(\frac{n\pi}{a}x) + B'\sin(\frac{n\pi}{a}x)]\sin(\frac{m\pi}{b}y)$
 $\vec{\nabla}_{\perp} \times \vec{B}_{\perp} = 0 \implies D' = 0, \quad B' = 0, \quad C' = A'\frac{n}{a}\frac{b}{m}$
 $\vec{\nabla}_{\perp} \cdot B_{\perp} = -ik_z B_z \cos(\frac{n\pi}{a}x)\cos(\frac{m\pi}{b}y) \implies A'\frac{b}{m\pi}k_{nm}^{(E)2} = -ik_z B_z$



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Cylindrical Wave Guides



TM Modes:

$$\begin{split} E_{z}(\vec{x}_{0}) &= 0 \quad \vec{\nabla}_{\perp}^{2} E_{z} = [k_{z}^{2} - (\frac{\omega}{c})^{2}] E_{z} \\ &(\partial_{r}^{2} + \frac{1}{r} \partial_{r} + \frac{1}{r^{2}} \partial_{\varphi}^{2}) E_{z} = [k_{z}^{2} - (\frac{\omega}{c})^{2}] E_{z} \\ &(\xi^{2} \partial_{\xi}^{2} + \xi \partial_{\xi} + \xi^{2} - n^{2}) E_{z} = 0, \quad \xi = k_{nm}^{(E)} r \\ &E_{z}(\vec{x}) = E_{z} J_{n} (k_{nm}^{(B)} r) e^{in\varphi} \qquad k_{nm}^{(B)} \text{ is the mth 0 of the nth Bessel function over r.} \end{split}$$

TE Modes:

 $\partial_r B_z(\vec{x}_0) = 0 \qquad \qquad \vec{\nabla}_{\perp}^2 B_z = [k_z^2 - (\frac{\omega}{c})^2] B_z$ $B_z(\vec{x}) = B_z J_n(k_{nm}^{(E)} r) e^{in\varphi} \qquad \qquad k_{nm}^{(E)} \text{ is the mth extremeum of } J_n \text{ over r.}$

Notation: TE_{nm} Mode



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Resonant Cavities



TE Modes: Standing waves with nodes

 $B_z(\vec{x}) \propto \sin(k_z z) \sin(\omega t), \quad k_z = \frac{l\pi}{L}$ l > 0

TM Modes: Standing waves with nodes

 $E_z(\vec{x}) \propto \cos(k_z z) \cos(\omega t), \quad k_z = \frac{l\pi}{L}$ $l \ge 0$



For each mode TE_{nm} or TM_{nm} there is a discrete set of frequencies that can be excited.

$$\omega_{nm}^{(E/B)} = c\sqrt{k_{nm}^{(E/B)2} + \left(\frac{l\pi}{L}\right)^2}$$



Resonant Cavities Examples



Rectangular cavity:





Cavity Operation



500MHz Cavity of DORIS:



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Superconducting Cavities







A bell with this Q would ring for a year.

- Very low wall losses.
- Therefore continuous operation is possible.
- Energy recovery becomes possible.

Normal conducting cavities

- Significant wall losses.
- Cannot operate continuously with appreciable fields.
- Energy recovery was therefore not possible.







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