

# x-z Tilt Due to Dispersion in RF Cavities

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## 1 Constructing transport matrix in terms of twiss parameters and dispersion

First construct a matrix  $T_{12}$  from point 1 to 2 with  $\vec{\eta}_1$  and  $\vec{\eta}_2$  and no RF between 1 and 2. The horizontal and longitudinal motion is described in terms of  $\beta, \alpha, \phi$ . Next write the matrix for the RF cavity with frequency  $\omega$  and voltage  $V$ . Compute the full turn at point 2.  $T = T_{21}T_{RF}T_{12}$ . The  $C_{11}$  element of the C matrix at point 1 will give the x-z coupling in terms of the dispersion  $\vec{\eta}_2$  at the observation point and  $\vec{\eta}_1$  at the cavity, and the phase advance from cavity (1) to observation point (2).

### 1.1 Matrix $T_{12}$ from $\vec{\eta}_1$ to $\vec{\eta}_2$

We start with

$$T_{12} = \begin{pmatrix} M_{12} & m_{12} \\ n_{12} & N_{12} \end{pmatrix} \quad (1)$$

and then

$$T_{12} \begin{pmatrix} \eta_1 \\ \eta'_1 \\ l \\ 1 \end{pmatrix} = \begin{pmatrix} \eta_2 \\ \eta'_2 \\ l \\ 1 \end{pmatrix} \quad (2)$$

$$\rightarrow M_{12} \begin{pmatrix} \eta_1 \\ \eta'_1 \end{pmatrix} + m_{12} \begin{pmatrix} l \\ 1 \end{pmatrix} = \begin{pmatrix} \eta_2 \\ \eta'_2 \end{pmatrix} \quad (3)$$

The first column of  $m$  is zero because  $\vec{x}$  is independent of  $l$ .

$$m_{12} = \begin{pmatrix} 0 & a \\ 0 & b \end{pmatrix} \quad (4)$$

Then from Equations 3 and 4 we get

$$\begin{pmatrix} a \\ b \end{pmatrix} = \begin{pmatrix} \eta_2 \\ \eta'_2 \end{pmatrix} - M_{12} \begin{pmatrix} \eta_1 \\ \eta'_1 \end{pmatrix}$$

or

$$m_{12} = \begin{pmatrix} 0 & \eta_2 \\ 0 & \eta'_2 \end{pmatrix} - M_{12} \begin{pmatrix} 0 & \eta_1 \\ 0 & \eta'_1 \end{pmatrix} \quad (5)$$

Both  $M_{12}$  and  $N_{12}$  can be written in terms of twiss parameters for horizontal and longitudinal motion at 1 and 2. We use the symplecticity of  $T_{12}$  to determine  $n_{12}$ . Since  $T^T S T = S$  we can write

$$\begin{aligned} \begin{pmatrix} M^T & n^T \\ m^T & N^T \end{pmatrix} \begin{pmatrix} s & 0 \\ 0 & s \end{pmatrix} \begin{pmatrix} M & m \\ n & N \end{pmatrix} &= \begin{pmatrix} s & 0 \\ 0 & s \end{pmatrix} \\ \begin{pmatrix} M^T & n^T \\ m^T & N^T \end{pmatrix} \begin{pmatrix} sM & sm \\ sn & sN \end{pmatrix} &= \begin{pmatrix} s & 0 \\ 0 & s \end{pmatrix} \\ \begin{pmatrix} M^T sM + n^T sn & M^T sm + n^T sN \\ m^T sM + N^T sn & m^T sm + N^T sN \end{pmatrix} &= \begin{pmatrix} s & 0 \\ 0 & s \end{pmatrix} \\ &\rightarrow n^T sN = -M^T sm \\ &\rightarrow n^T = M^T sm N^{-1} s \end{aligned}$$

and

$$\rightarrow N^T sn = -m^T sM \quad (6)$$

$$\rightarrow n = s(N^T)^{-1} m^T sM \quad (7)$$

where in the last line we use  $s^{-1} = -s$ .

Now substitute  $m_{12}$  from Equation 4 for  $m$  in Equation 7 and we have

$$\begin{aligned} \rightarrow n^T &= M^T s \left( \begin{pmatrix} 0 & \eta_2 \\ 0 & \eta'_2 \end{pmatrix} - M \begin{pmatrix} 0 & \eta_1 \\ 0 & \eta'_1 \end{pmatrix} \right) N^{-1} s \\ &= \left( M^T s \begin{pmatrix} 0 & \eta_2 \\ 0 & \eta'_2 \end{pmatrix} - s \begin{pmatrix} 0 & \eta_1 \\ 0 & \eta'_1 \end{pmatrix} \right) N^{-1} s \end{aligned}$$

We can write  $M$  and  $N$  in terms of  $\beta$  and  $\alpha$  at 1 and 2 and  $\phi_{12}$ , the phase advance from one to the other. For simplicity let's suppose that  $\alpha_1 = \alpha_2 = 0$  and that  $\beta_1 = \beta_2$ . Then

$$M = \begin{pmatrix} \cos \mu_x & \beta_x \sin \mu_x \\ -\frac{\sin \mu_x}{\beta_x} & \cos \mu_x \end{pmatrix} \quad (8)$$

and for  $N$ ,  $x \rightarrow z$ . But we know that  $N$  has the form

$$N = \begin{pmatrix} 1 & \alpha_{12} \\ 0 & 1 \end{pmatrix} \quad (9)$$

since as there are no RF cavities between points 1 and 2, there is no change to the

energy. Then

$$\begin{aligned} \rightarrow n^T &= \left( \left( \begin{array}{cc} \cos \mu_x & -\frac{\sin \mu_x}{\beta_x} \\ \beta_x \sin \mu_x & \cos \mu_x \end{array} \right) \begin{pmatrix} 0 & 1 \\ -1 & 0 \end{pmatrix} \begin{pmatrix} 0 & \eta_2 \\ 0 & \eta'_2 \end{pmatrix} - \begin{pmatrix} 0 & 1 \\ -1 & 0 \end{pmatrix} \begin{pmatrix} 0 & \eta_1 \\ 0 & \eta'_1 \end{pmatrix} \right) \begin{pmatrix} 1 & -\alpha_{12} \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 0 & 1 \\ -1 & 0 \end{pmatrix} \\ &= \left( \left( \begin{array}{cc} \frac{\sin \mu_x}{\beta_x} & \cos \mu_x \\ -\cos \mu_x & \beta_x \sin \mu_x \end{array} \right) \begin{pmatrix} 0 & \eta_2 \\ 0 & \eta'_2 \end{pmatrix} - \begin{pmatrix} 0 & \eta'_1 \\ 0 & -\eta_1 \end{pmatrix} \right) \begin{pmatrix} \alpha_{12} & 1 \\ -1 & 0 \end{pmatrix} \end{aligned} \quad (10)$$

$$= \left( \begin{pmatrix} 0 & \frac{\sin \mu_x}{\beta_x} \eta_2 + \cos \mu_x \eta'_2 \\ 0 & -\cos \mu_x \eta_2 + \beta_x \sin \mu_x \eta'_2 \end{pmatrix} - \begin{pmatrix} 0 & \eta'_1 \\ 0 & -\eta_1 \end{pmatrix} \right) \begin{pmatrix} \alpha_{12} & 1 \\ -1 & 0 \end{pmatrix} \quad (11)$$

$$= \begin{pmatrix} 0 & \frac{\sin \mu_x}{\beta_x} \eta_2 + \cos \mu_x \eta'_2 - \eta'_1 \\ 0 & -\cos \mu_x \eta_2 + \beta_x \sin \mu_x \eta'_2 + \eta_1 \end{pmatrix} \begin{pmatrix} \alpha_{12} & 1 \\ -1 & 0 \end{pmatrix} \quad (12)$$

$$= \begin{pmatrix} -\frac{\sin \mu_x}{\beta_x} \eta_2 - \cos \mu_x \eta'_2 + \eta'_1 & 0 \\ \cos \mu_x \eta_2 - \beta_x \sin \mu_x \eta'_2 - \eta_1 & 0 \end{pmatrix} \quad (13)$$

$$\rightarrow n = \begin{pmatrix} -\frac{\sin \mu_x}{\beta_x} \eta_2 - \cos \mu_x \eta'_2 + \eta'_1 & \cos \mu_x \eta_2 - \beta_x \sin \mu_x \eta'_2 - \eta_1 \\ 0 & 0 \end{pmatrix} \quad (14)$$

## 2 RF cavity

The matrix for an RF cavity is

$$N_{RF} = \begin{pmatrix} 1 & 0 \\ e^{\frac{L\omega}{c}V} & 1 \end{pmatrix} \quad (15)$$

The full turn matrix for the longitudinal motion is

$$N = \begin{pmatrix} 1 & \alpha_p \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ \tilde{V} & 1 \end{pmatrix} = \begin{pmatrix} 1 + \alpha_p \tilde{V} & L\alpha_p \\ \tilde{V} & 1 \end{pmatrix} \quad (16)$$

Then  $\cos \mu_z = 1 + \frac{1}{2} \frac{\alpha_p \omega V L}{c E_{beam}}$  and  $\mu_z \sim \sqrt{\frac{\alpha_p \omega V L}{c E_{beam}}}$ . And

$$\begin{aligned} \beta_z \sin \mu_z &= L\alpha_p \\ \rightarrow \beta_z &= \frac{L\alpha_p}{\mu_z} \end{aligned}$$

We can evaluate the full turn matrix at an arbitrary point

$$\begin{aligned} T_{arb} &= \begin{pmatrix} 1 & \alpha_{12} \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ \tilde{V} & 1 \end{pmatrix} \begin{pmatrix} 1 & \alpha_{21} \\ 0 & 1 \end{pmatrix} \\ &= \begin{pmatrix} 1 + \tilde{V}\alpha_{12} & \alpha_{12} \\ \tilde{V} & 1 \end{pmatrix} \begin{pmatrix} 1 & \alpha_{21} \\ 0 & 1 \end{pmatrix} \\ &= \begin{pmatrix} 1 + \tilde{V}\alpha_{12} & (1 + \tilde{V}\alpha_{12})\alpha_{21} + \alpha_{12} \\ \tilde{V} & \tilde{V}\alpha_{21} + 1 \end{pmatrix} \end{aligned}$$

Since  $\alpha_{12} + \alpha_{21} = \alpha$ , we see that to first order in  $\alpha$ ,  $\beta_z$  is about the same.

### 3 Full turn

$$\begin{aligned}
T &= \begin{pmatrix} M_{12} & m_{12} \\ n_{12} & N_{12} \end{pmatrix} \begin{pmatrix} I & 0 \\ 0 & N_{RF} \end{pmatrix} \begin{pmatrix} M_{21} & m_{21} \\ n_{21} & N_{21} \end{pmatrix} \\
&= \begin{pmatrix} M_{12} & m_{12} \\ n_{12} & N_{12} \end{pmatrix} \begin{pmatrix} M_{21} & m_{21} \\ N_{RF} n_{21} & N_{RF} N_{21} \end{pmatrix} \\
\begin{pmatrix} M & m \\ n & N \end{pmatrix} &= \begin{pmatrix} M_{12} M_{21} + m_{12} N_{RF} n_{21} & M_{12} m_{21} + m_{12} N_{RF} N_{21} \\ n_{12} M_{21} + N_{12} N_{RF} n_{21} & n_{12} m_{21} + N_{12} N_{RF} N_{21} \end{pmatrix}
\end{aligned}$$

### 4 C-matrix

The coupling matrix

$$\begin{aligned}
C &\propto m + n^\dagger = M_{12} m_{21} + m_{12} N_{RF} N_{21} + (n_{12} M_{21} + N_{12} N_{RF} n_{21})^\dagger \\
&= \begin{pmatrix} \cos \mu_{12} & \beta_x \sin \mu_{12} \\ -\frac{\sin \mu_{12}}{\beta_x} & \cos \mu_{12} \end{pmatrix} \begin{pmatrix} 0 & a_{21} \\ 0 & b_{21} \end{pmatrix} + \begin{pmatrix} 0 & a_{12} \\ 0 & b_{12} \end{pmatrix} \begin{pmatrix} 1 & 0 \\ \tilde{V} & 1 \end{pmatrix} \begin{pmatrix} 1 & \alpha_{21} \\ 0 & 1 \end{pmatrix} \\
&\quad + \left( \begin{pmatrix} c_{12} & d_{12} \\ 0 & 0 \end{pmatrix} \begin{pmatrix} \cos \mu_{21} & \beta_x \sin \mu_{21} \\ -\frac{\sin \mu_{21}}{\beta_x} & \cos \mu_{21} \end{pmatrix} + \begin{pmatrix} 1 & \alpha_{12} \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ \tilde{V} & 1 \end{pmatrix} \begin{pmatrix} c_{21} & d_{21} \\ 0 & 0 \end{pmatrix} \right)^\dagger \\
&= \begin{pmatrix} 0 & a_{21} \cos \mu_{12} + b_{21} \beta_x \sin \mu_{12} \\ 0 & -a_{21} \frac{\sin \mu_{12}}{\beta_x} + b_{21} \cos \mu_{12} \end{pmatrix} + \begin{pmatrix} 0 & a_{12} \\ 0 & b_{12} \end{pmatrix} \begin{pmatrix} 1 & \alpha_{12} \\ \tilde{V} & \tilde{V} \alpha_{21} + 1 \end{pmatrix} \\
&\quad + \left( \begin{pmatrix} c_{12} \cos \mu_{21} - d_{12} \frac{\sin \mu_{21}}{\beta_x} & c_{12} \beta_x \sin \mu_{21} + d_{12} \cos \mu_{21} \\ 0 & 0 \end{pmatrix} + \begin{pmatrix} 1 & \alpha_{12} \\ 0 & 1 \end{pmatrix} \begin{pmatrix} c_{21} & d_{21} \\ \tilde{V} c_{21} & \tilde{V} d_{21} \end{pmatrix} \right)^\dagger \\
&= \begin{pmatrix} 0 & a_{21} \cos \mu_{12} + b_{21} \beta_x \sin \mu_{12} \\ 0 & -a_{21} \frac{\sin \mu_{12}}{\beta_x} + b_{21} \cos \mu_{12} \end{pmatrix} + \begin{pmatrix} a_{12} \tilde{V} & a_{12} (\tilde{V} \alpha_{21} + 1) \\ b_{12} \tilde{V} & b_{12} (\tilde{V} \alpha_{21} + 1) \end{pmatrix} \\
&\quad + \left( \begin{pmatrix} c_{12} \cos \mu_{21} - d_{12} \frac{\sin \mu_{21}}{\beta_x} & c_{12} \beta_x \sin \mu_{21} + d_{12} \cos \mu_{21} \\ 0 & 0 \end{pmatrix} + \begin{pmatrix} 1 & \alpha_{12} \\ 0 & 1 \end{pmatrix} \begin{pmatrix} c_{21} & d_{21} \\ \tilde{V} c_{21} & \tilde{V} d_{21} \end{pmatrix} \right)^\dagger \\
&= \begin{pmatrix} a_{12} \tilde{V} & a_{21} \cos \mu_{12} + b_{21} \beta_x \sin \mu_{12} + a_{12} (\tilde{V} \alpha_{21} + 1) \\ b_{12} \tilde{V} & -a_{21} \frac{\sin \mu_{12}}{\beta_x} + b_{21} \cos \mu_{12} + b_{12} (\tilde{V} \alpha_{21} + 1) \end{pmatrix} \\
&\quad + \begin{pmatrix} 0 & -c_{12} \beta_x \sin \mu_{21} - d_{12} \cos \mu_{21} \\ 0 & c_{12} \cos \mu_{21} - d_{12} \frac{\sin \mu_{21}}{\beta_x} \end{pmatrix} + \begin{pmatrix} c_{12} + \alpha_{12} \tilde{V} c_{21} & d_{12} + \alpha_{12} \tilde{V} d_{21} \\ \tilde{V} c_{12} & \tilde{V} d_{12} \end{pmatrix}^\dagger \\
&= \begin{pmatrix} a_{12} \tilde{V} & a_{21} \cos \mu_{12} + b_{21} \beta_x \sin \mu_{12} + a_{12} (\tilde{V} \alpha_{21} + 1) \\ b_{12} \tilde{V} & -a_{21} \frac{\sin \mu_{12}}{\beta_x} + b_{21} \cos \mu_{12} + b_{12} (\tilde{V} \alpha_{21} + 1) \end{pmatrix} \\
&\quad + \begin{pmatrix} 0 & -c_{12} \beta_x \sin \mu_{21} - d_{12} \cos \mu_{21} \\ 0 & c_{12} \cos \mu_{21} - d_{12} \frac{\sin \mu_{21}}{\beta_x} \end{pmatrix} + \begin{pmatrix} \tilde{V} d_{21} & -d_{12} - \alpha_{12} \tilde{V} d_{21} \\ -\tilde{V} c_{12} & c_{12} + \alpha_{12} \tilde{V} c_{21} \end{pmatrix}
\end{aligned}$$

Finally just picking out  $C_{11}$

$$C_{11} = (a_{12} + d_{21})\tilde{V} \quad (17)$$

We get  $a_{12}$  from Equation 5 and  $d_{21}$  from Equation 14, where we are again assuming  $\beta_1 = \beta_2$  and  $\alpha_1 = \alpha_2 = 0$ .

$$\begin{aligned} a_{12} &= \eta_2 - \cos \mu_{12}\eta_1 - \beta_x \sin \mu_{12}\eta'_1 \\ d_{21} &= \cos \mu_{21}\eta_1 - \beta_x \sin \mu_{21}\eta'_1 - \eta_2 \end{aligned}$$

and

$$C_{11} = ((\cos \mu_{21} - \cos \mu_{12})\eta_1 - \beta_x \eta'_1 (\sin \mu_{12} + \sin \mu_{21})) \tilde{V} \quad (18)$$

## 5 $\beta_1 \neq \beta_2$

Return to Equation 5 to get  $a_{12}$

$$\begin{aligned} m_{12} &= \begin{pmatrix} 0 & \eta_2 \\ 0 & \eta'_2 \end{pmatrix} - M_{12} \begin{pmatrix} 0 & \eta_1 \\ 0 & \eta'_1 \end{pmatrix} \\ m_{12} &= \begin{pmatrix} 0 & \eta_2 \\ 0 & \eta'_2 \end{pmatrix} - \begin{pmatrix} \sqrt{\frac{\beta_2}{\beta_1}} \cos \mu & \sqrt{\beta_1 \beta_2} \sin \mu \\ -\frac{\sin \mu}{\beta_1 \beta_2} & \sqrt{\frac{\beta_1}{\beta_2}} \cos \mu \end{pmatrix} \begin{pmatrix} 0 & \eta_1 \\ 0 & \eta'_1 \end{pmatrix} \\ \rightarrow a_{12} &= \eta_2 - \sqrt{\frac{\beta_2}{\beta_1}} \cos \mu_{12}\eta_1 - \sqrt{\beta_1 \beta_2} \sin \mu_{12}\eta'_1 \end{aligned}$$

and then to Equation 14 to get  $d_{12}$

$$d_{21} = \sqrt{\frac{\beta_2}{\beta_1}} \cos \mu_{21}\eta_1 - \sqrt{\beta_1 \beta_2} \sin \mu_{21}\eta'_1 - \eta_2 \quad (19)$$

Then

$$C_{11} = \left( \sqrt{\frac{\beta_2}{\beta_1}} (\cos \mu_{21} - \cos \mu_{12})\eta_1 - \sqrt{\beta_1 \beta_2} \eta'_1 (\sin \mu_{12} + \sin \mu_{21}) \right) \tilde{V} \quad (20)$$

## 6 Both RF Cavities

East and west RF cavities are approximately symmetric with respect to the IP ( $\mu = 0$ ). The  $C_{11}$  element of each is

$$\begin{aligned} C_{11}^W &= \left( \sqrt{\frac{\beta_2}{\beta_1}} (\cos \mu_{21} - \cos \mu_{12})\eta_1 - \sqrt{\beta_1 \beta_2} \eta'_1 (\sin \mu_{12} + \sin \mu_{21}) \right) \tilde{V} \\ C_{11}^E &\propto \left( \sqrt{\frac{\beta_2}{\beta_1}} (\cos(\mu_{21} - \Delta\mu) - \cos(\mu_{12} + \Delta\mu))\eta_1 + \sqrt{\beta_1 \beta_2} \eta'_1 (\sin(\mu_{12} + \Delta\mu) + \sin(\mu_{21} - \Delta\mu)) \right) \tilde{V} \end{aligned}$$

where  $\Delta\mu$  is the phase advance between the cavities along the path that does not include point 2, and  $\eta'_E = -\eta'_W$ . Then

$$C_{11}(2) \propto \left( \sqrt{\frac{\beta_2}{\beta_1}} (\cos \mu_{21} - \cos \mu_{12} + \cos(\mu_{21} - \Delta\mu) - \cos(\mu_{12} + \Delta\mu)) \eta_1 - \sqrt{\beta_1 \beta_2} \eta'_1 (\sin \mu_{12} + \sin \mu_{21} - \sin(\mu_{12} + \Delta\mu) - \sin(\mu_{21} - \Delta\mu)) \right) \tilde{V}$$