

# LITHIUM LENS STUDIES

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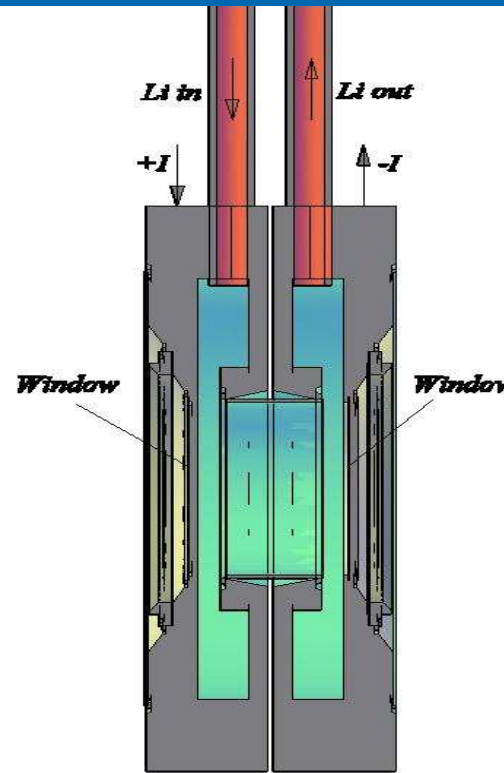
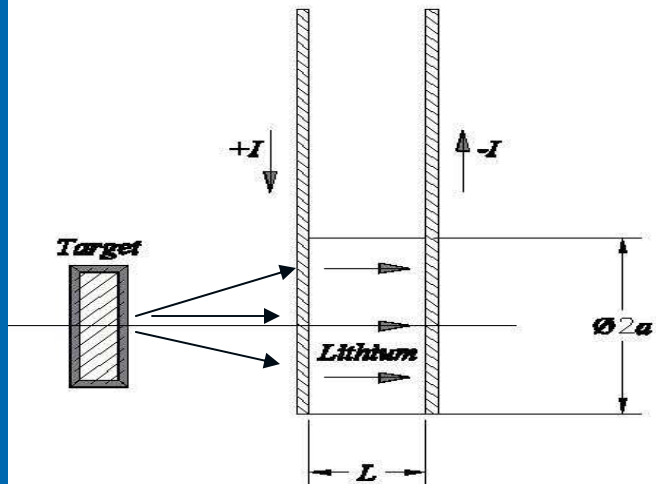
Linear Collider Workshop of Americas

ALCPG , September 30, 2009

Albuquerque NM

# LI LENS BASICS

Beam and current are moving co-directionally



Li also serves as a coolant for windows

Windows made from BN, BC or Be

W is also under consideration for entrance window

For given focal distance  $F$ , radius  $a$ , length  $L$ , the current required is

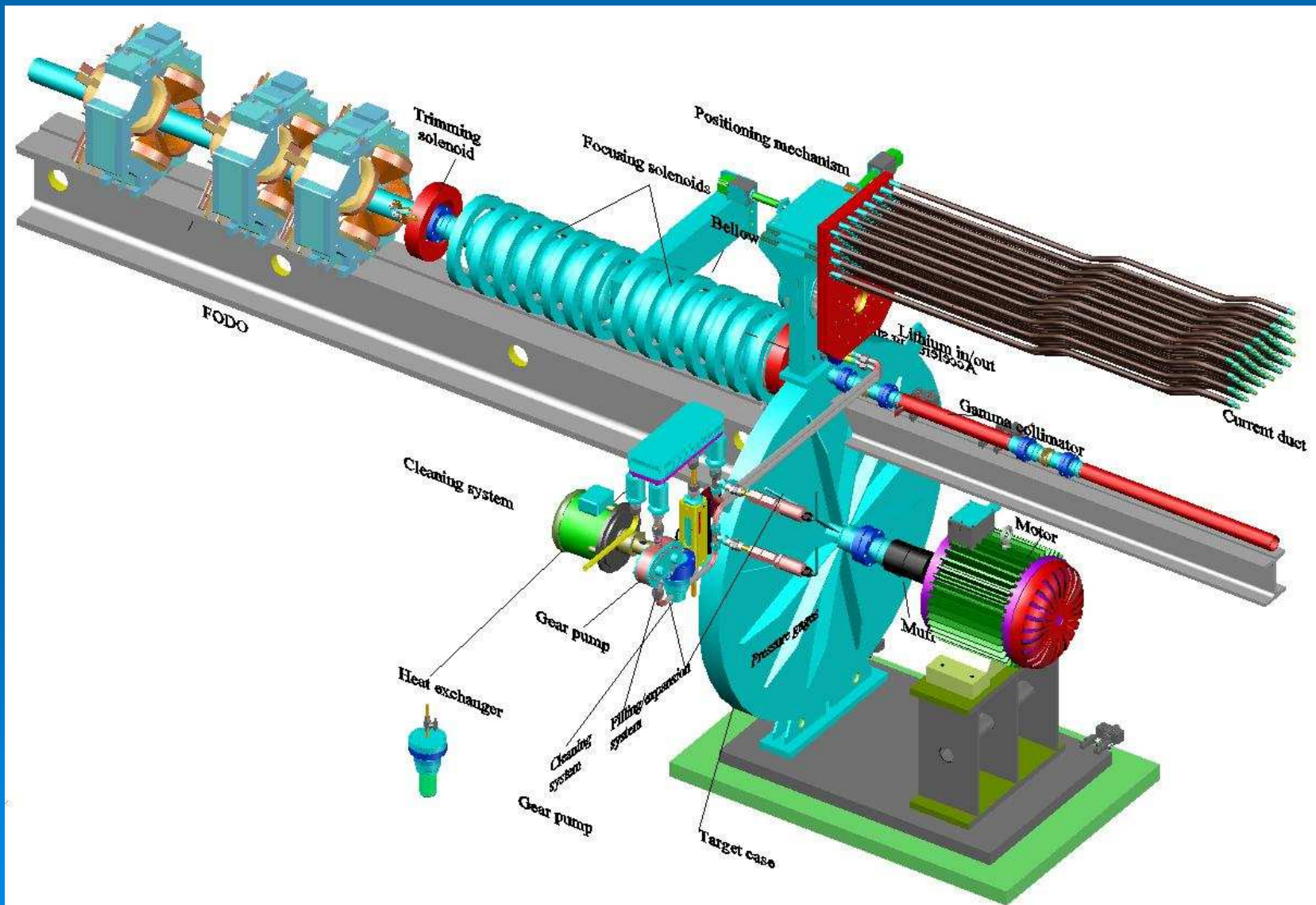
$$I \cong \frac{a^2 \cdot (HR)}{0.2FL}$$

For  $F \sim 1\text{cm}$ ,  $a \sim 0.5\text{cm}$ ,  $L \sim 0.5\text{cm}$ ,  $E \sim 20\text{MeV} \rightarrow I \sim 166\text{kA}$

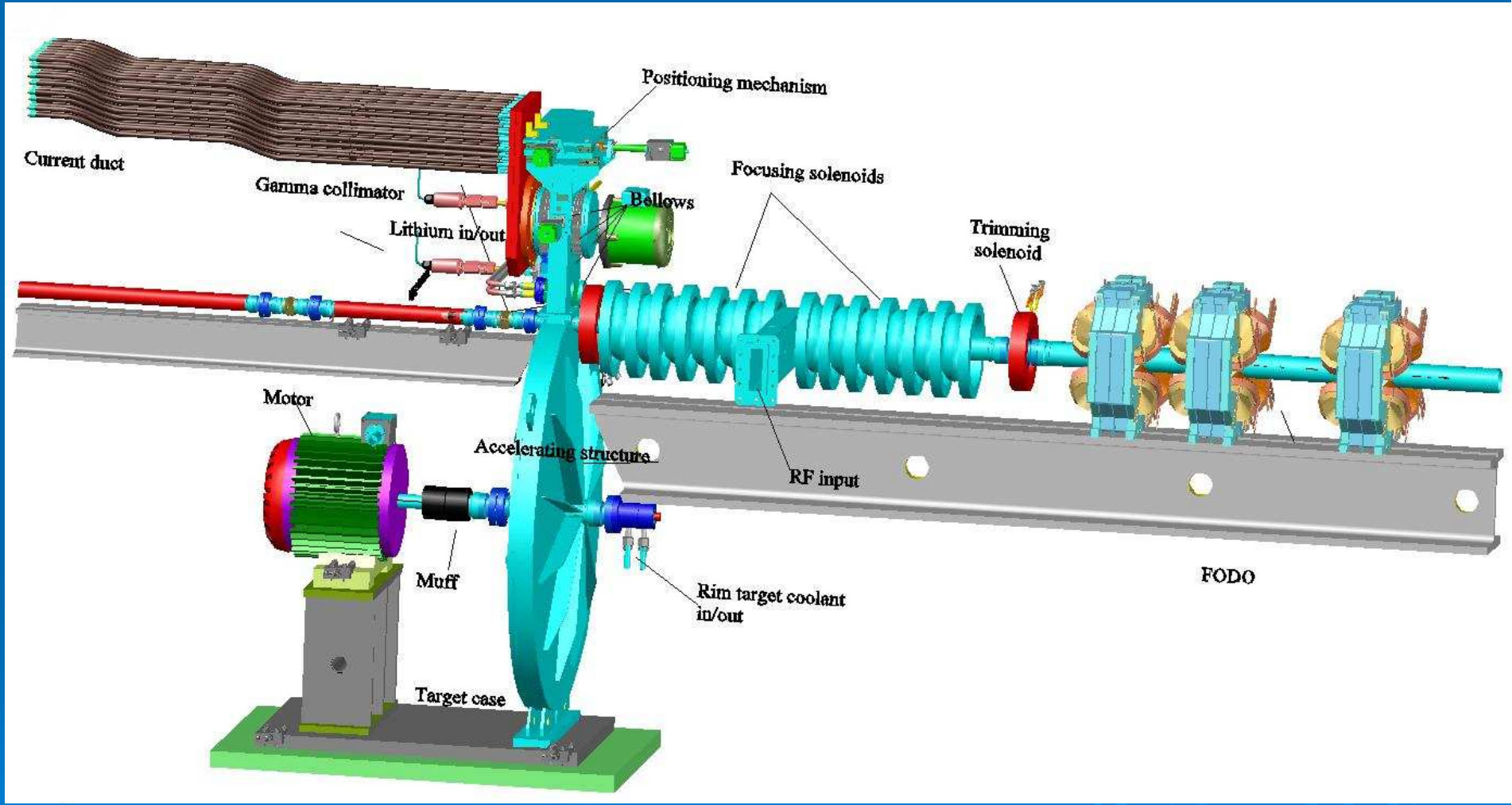
A.Mikhailichenko," Lithium Lens (I)", CBN -09-4, Aug 2009, 17pp.

<http://www.lepp.cornell.edu/public/CBN/2009/CBN09-4/CBN%2009-04.pdf>

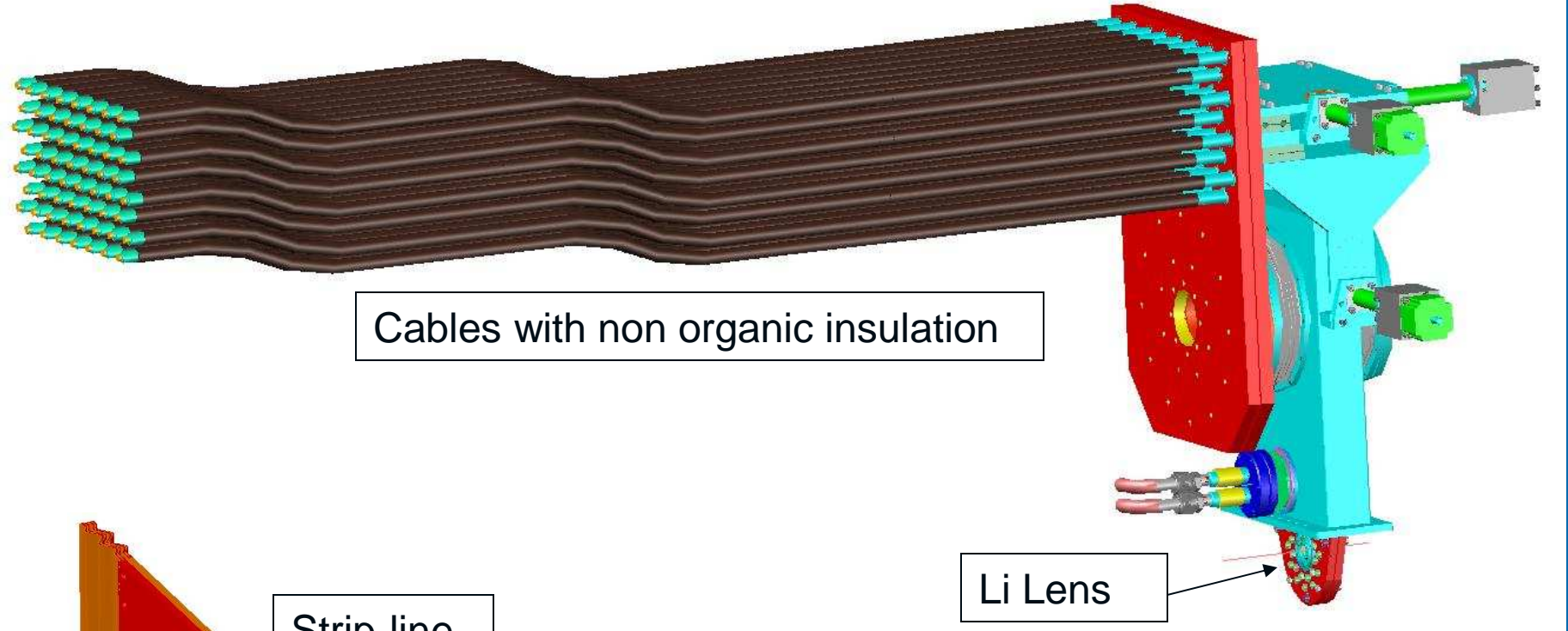
All references are there



# View from other side

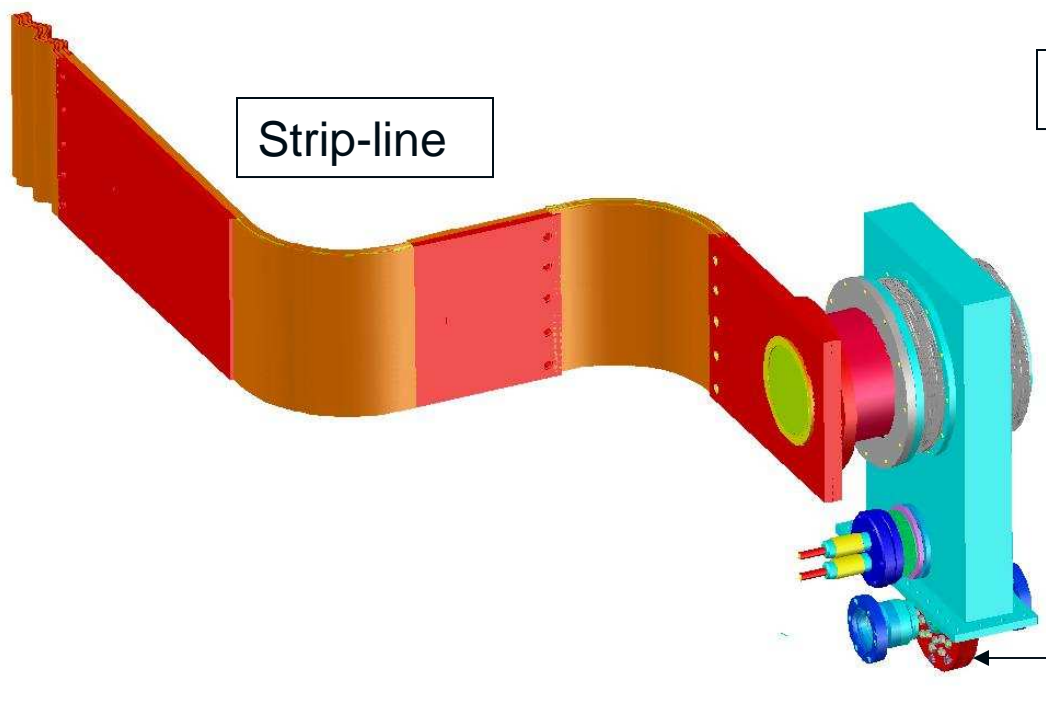


## Variants of current duct



Cables with non organic insulation

Li Lens

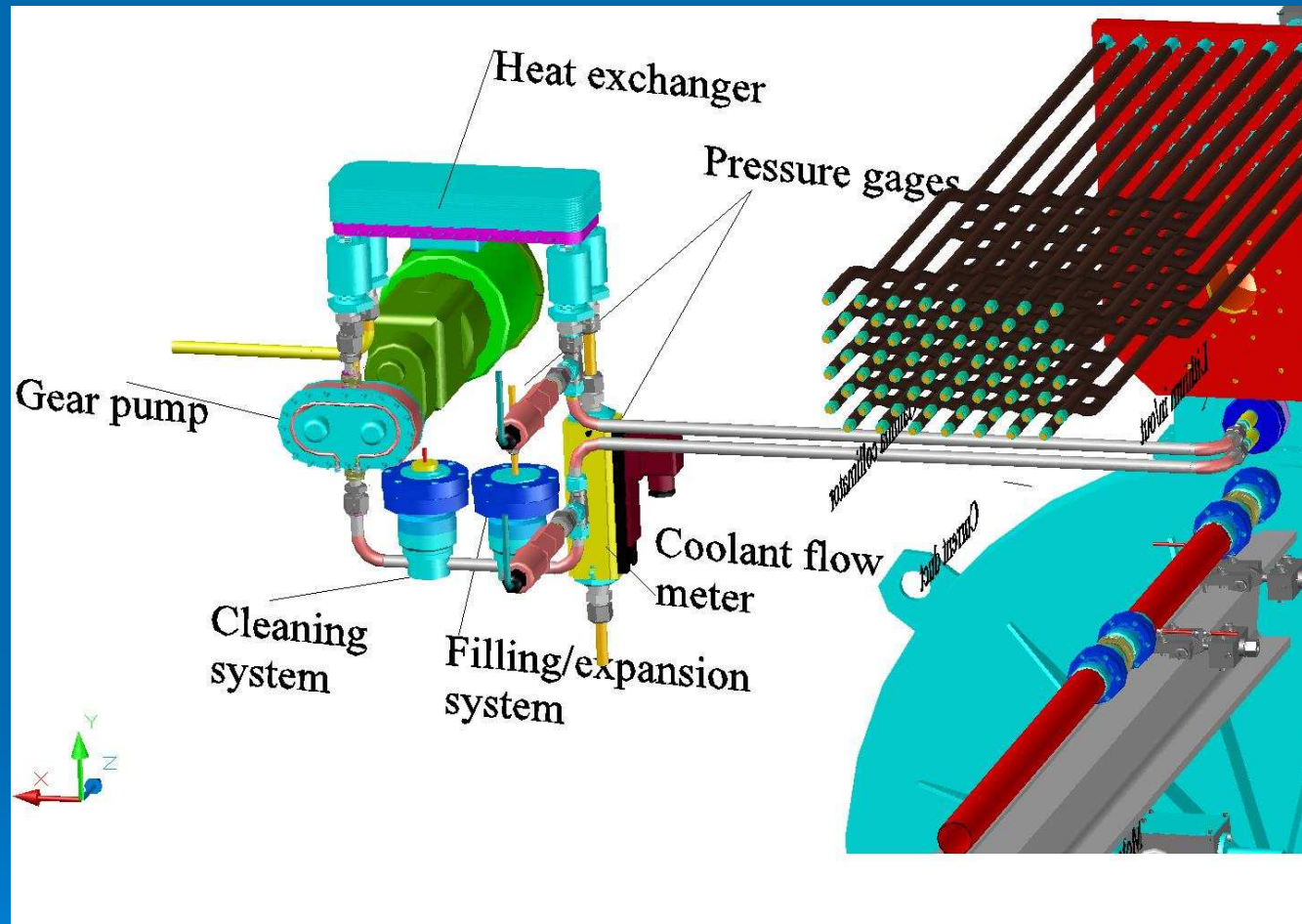


Strip-line

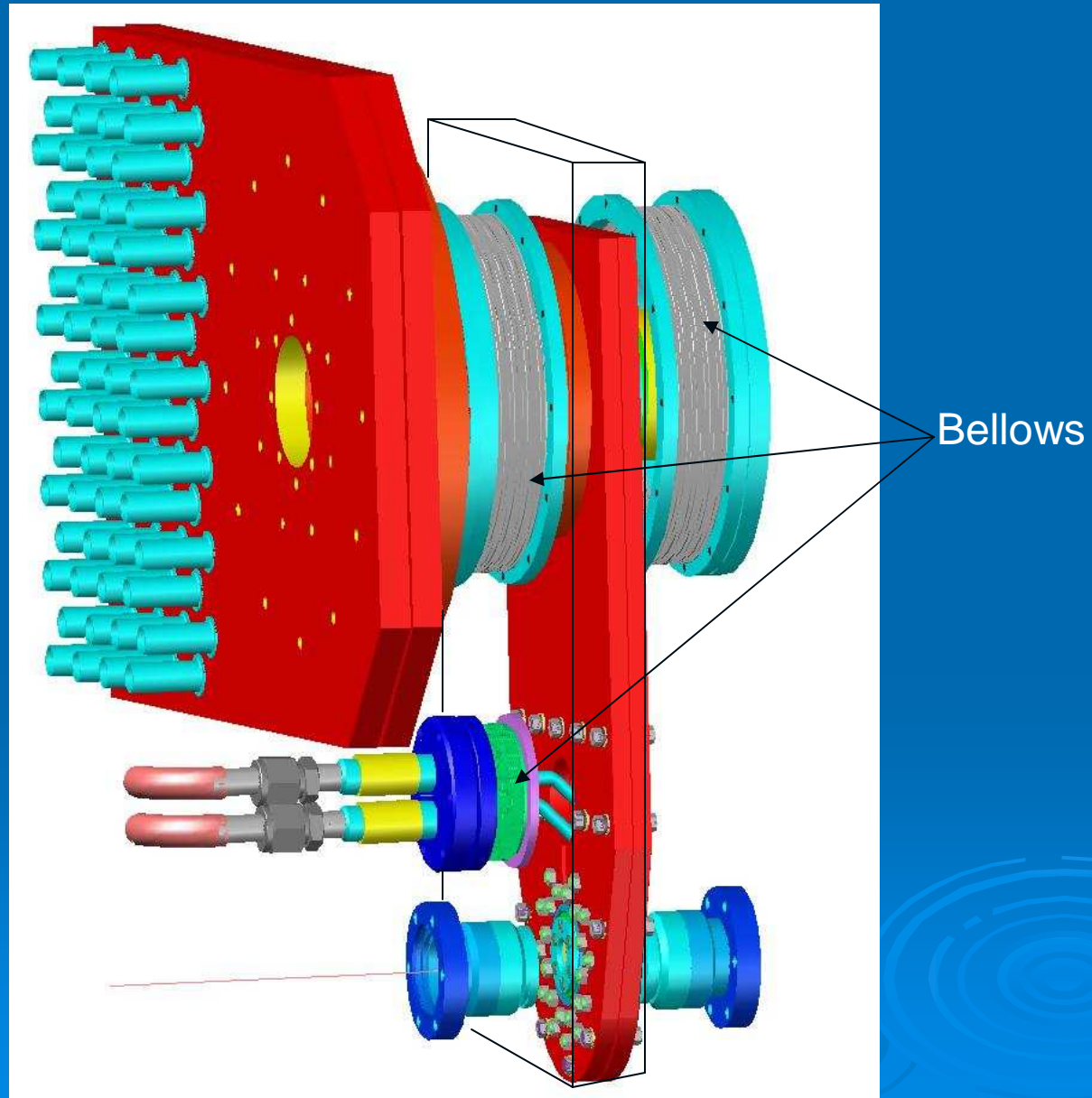
Li lens

Current duct must be able to transfer  $\sim 150$  kA in  $\sim 4$  ms pulse with repetition rate up to 10 Hz

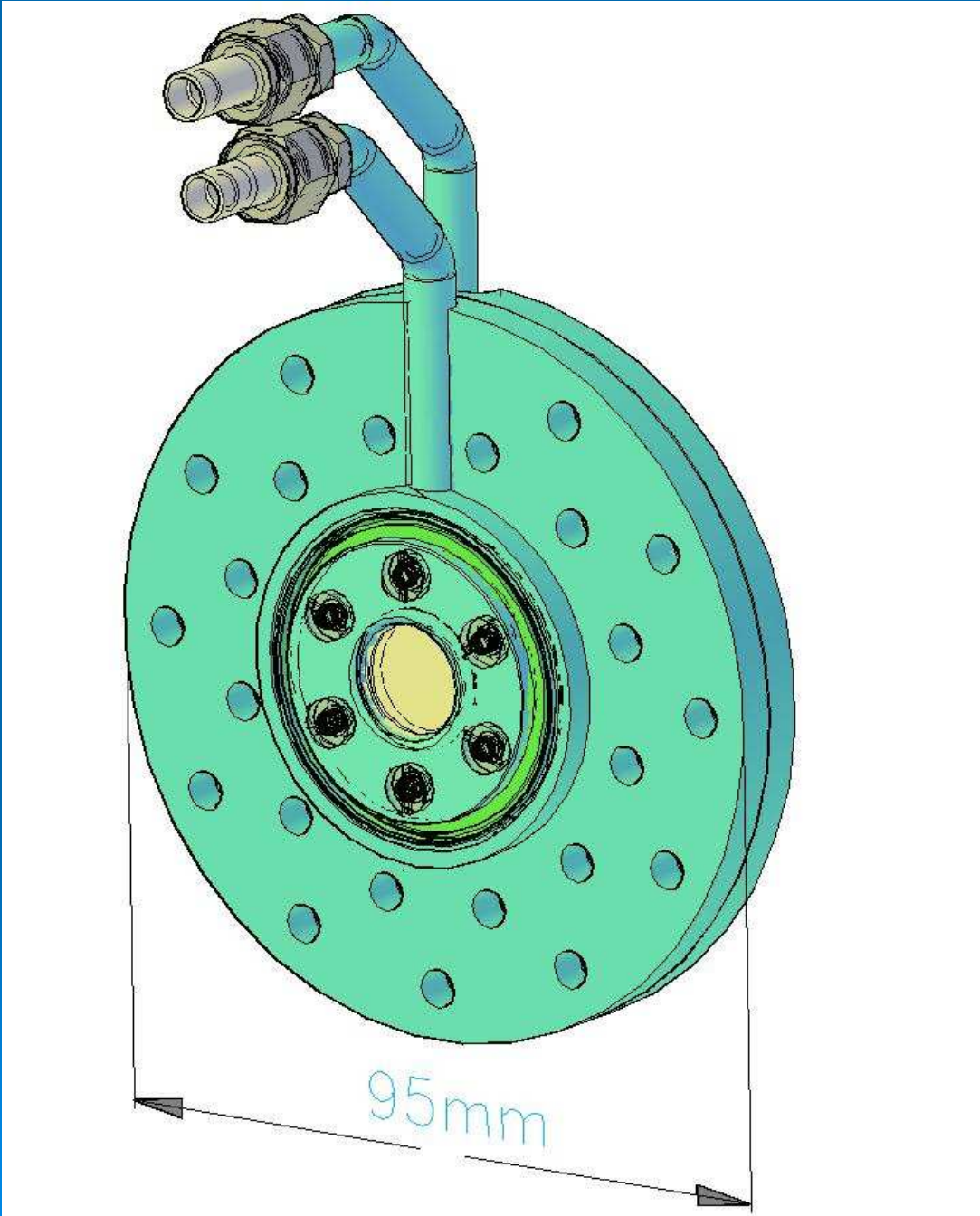
# Lithium loop



Scaled view on vacuumed feed through and lens; vacuum case not shown

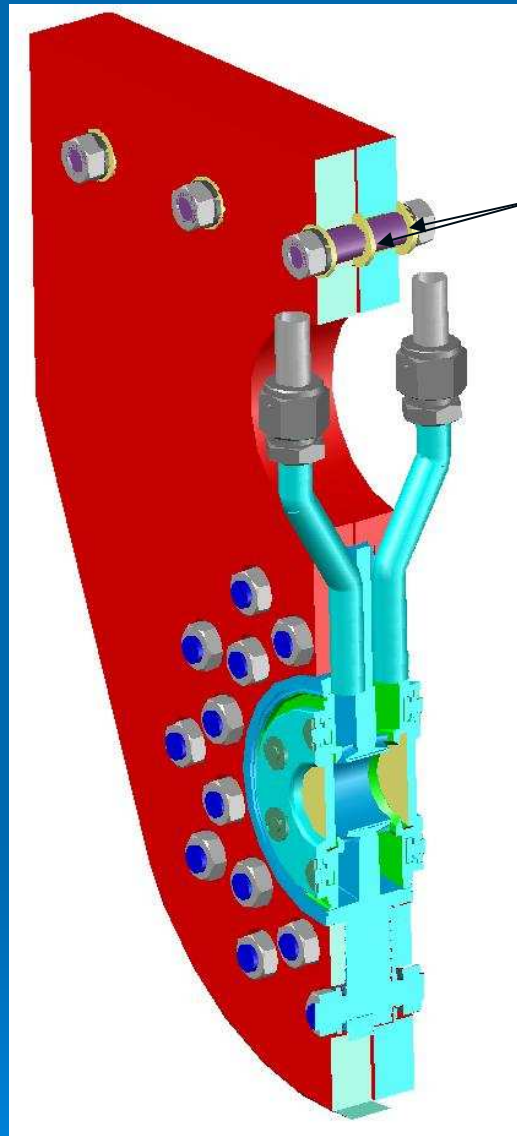


Lens itself

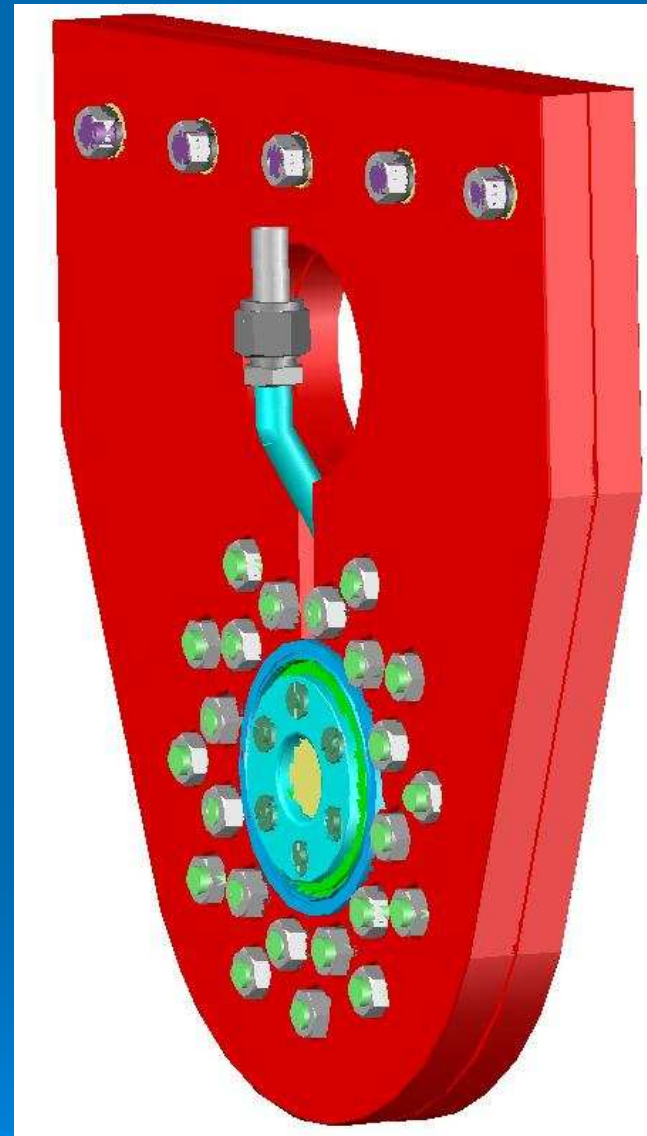




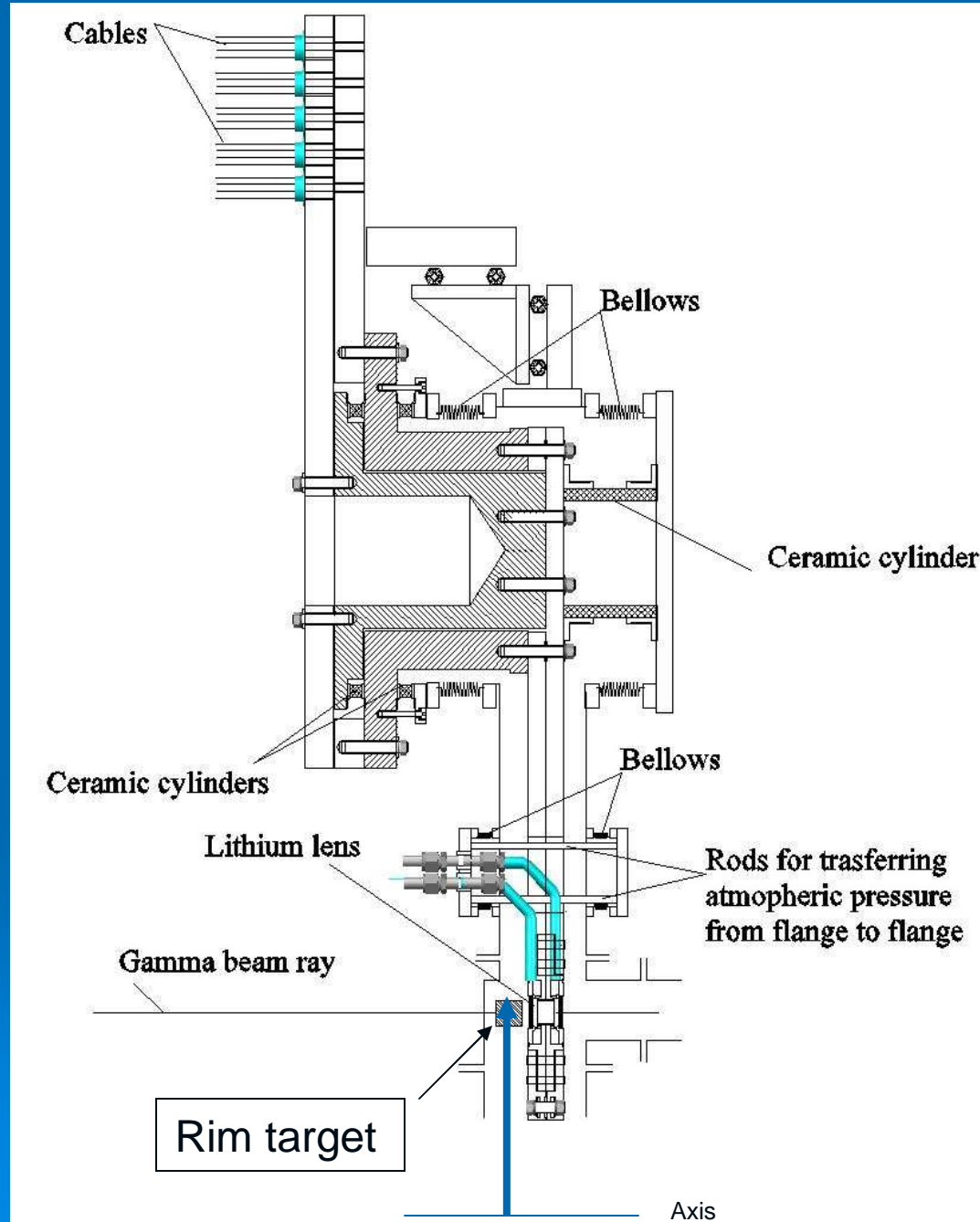
# Li lens with current duct attached



Ceramic washes



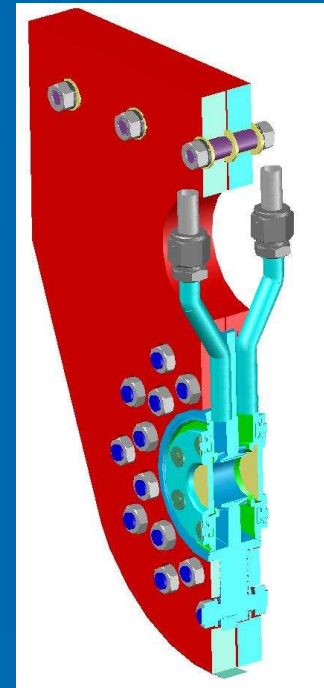
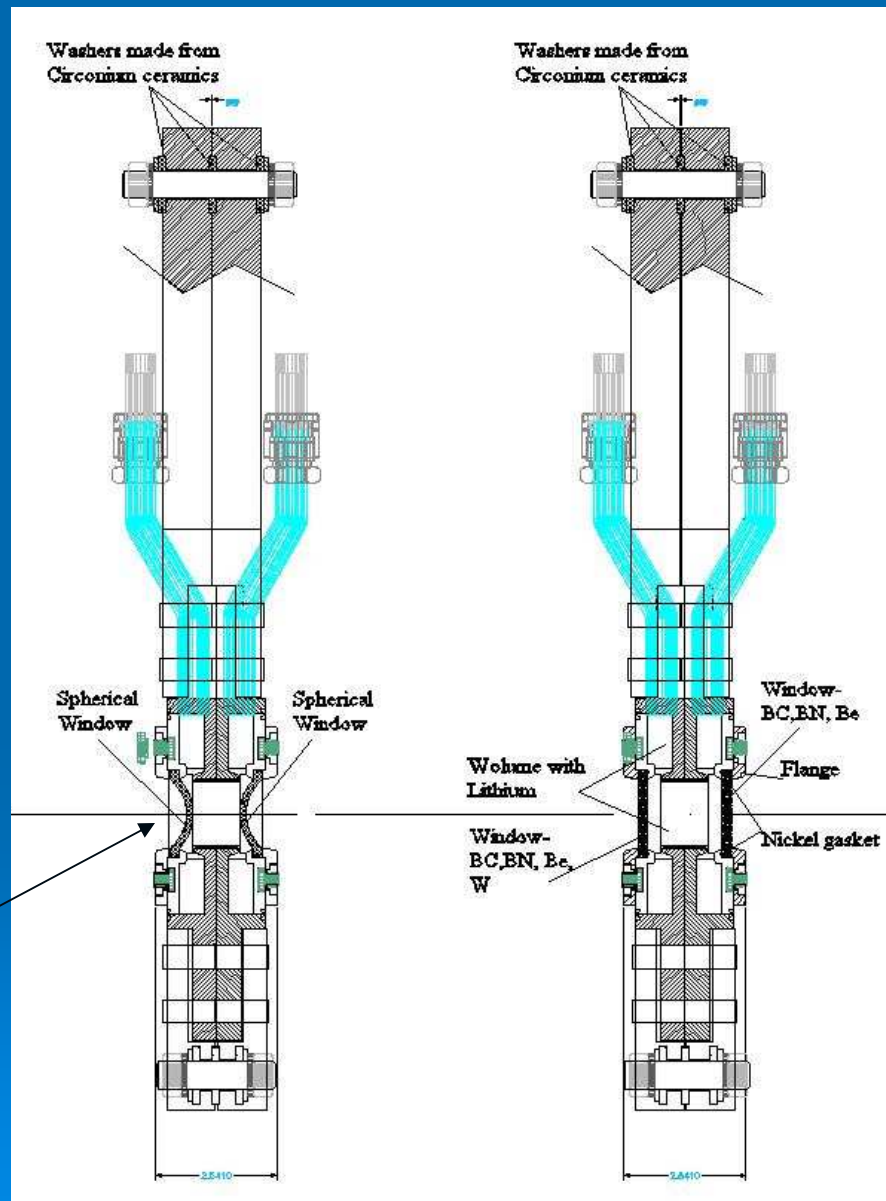
## FEED THROUGH IN DETAIL



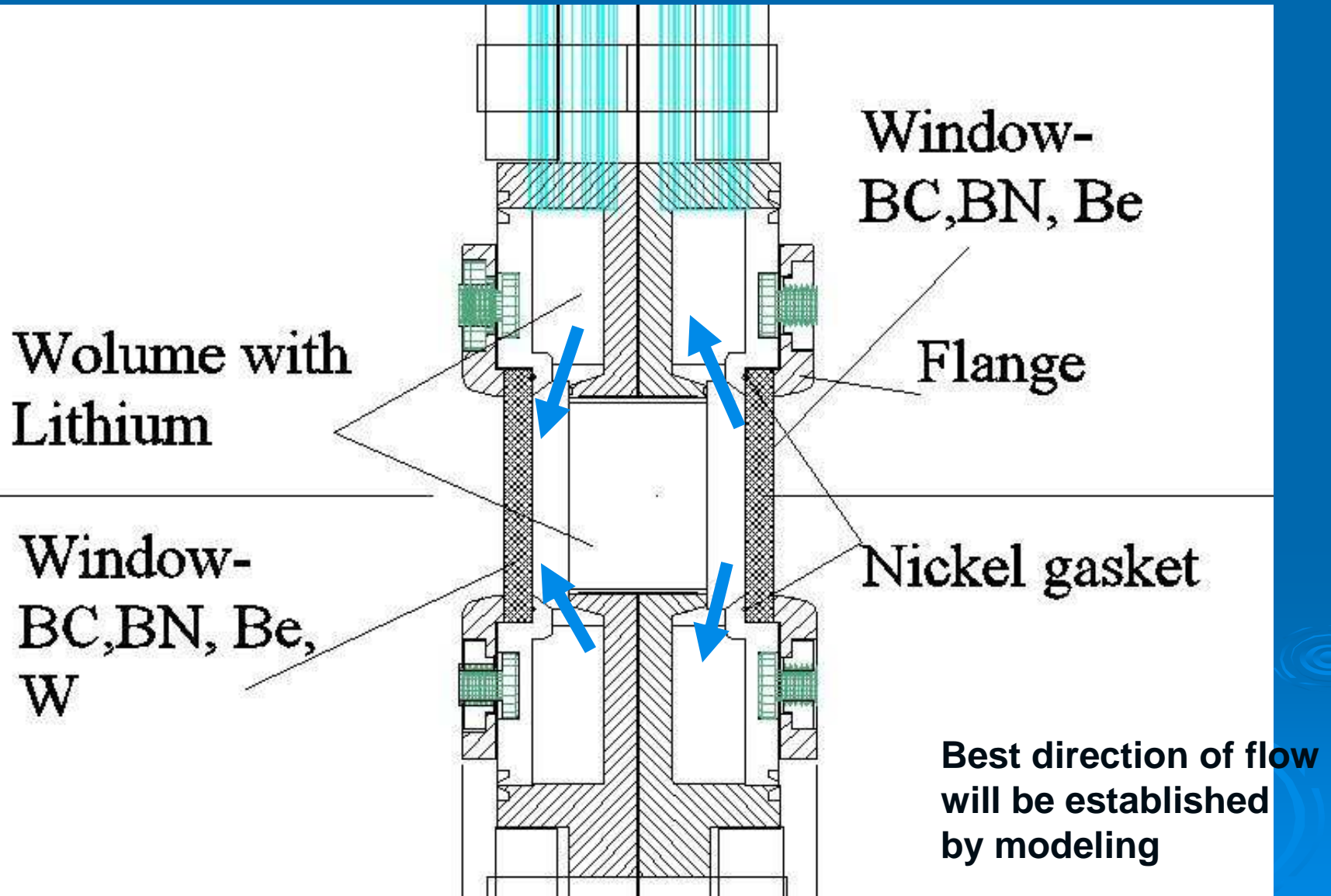
System with two bellows excludes net force from atmospheric pressure;

Positioning system serves for adjustment the distance between target and lens – what is required by optimization of yield/heating for the entrance window

Can be used for compensation of spherical aberrations



# Windows attachment technique



## To the choice of material for windows

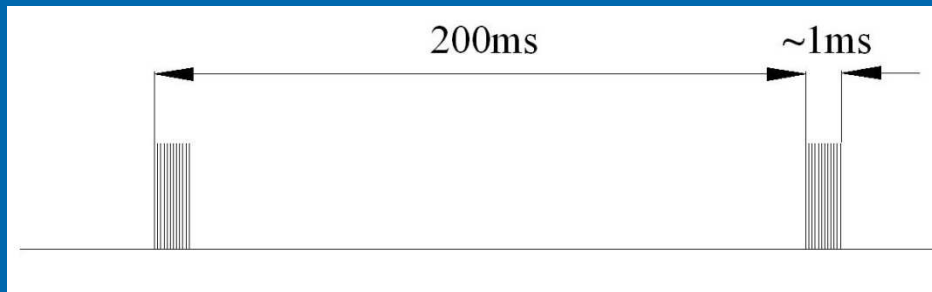
Table 1: properties of Lithium, Li<sup>1</sup>, Be, BC, BN, W

	Units	Li	Be	BN	B <sub>4</sub> C	W
Atomic number, $Z$	-	3	4	5/7	5/6	74
Yong modulus	$GPa$	4.9	287	350-400	450	400
Density, $\rho$	$[g/cm^3]$	0.533	1.846	3.487	2.52	19.254
Specific resistance	$Ohm-cm$	$1.44 \times 10^{-5}$	$1.9 \times 10^{-5}$	$>10^{14}$	$7.14 \times 10^{-3}$	$5.5 \times 10^{-6}$
Length of Xo, $IXo$	$cm$	152.1	34.739	27.026	19.88	0.35
Boil temperature	$^{\circ}C$	1347	2469	Sublimation	3500	5660
Melt temperature	$^{\circ}C$	180.54	1287	2973	2350	3410
Compressibility	$cm^2/kg$	$8.7 \times 10^{-6}$	$9.27 \times 10^{-7}$			$2.93 \times 10^{-7}$
Grüneisen coeff.	-					2.4
Speed of sound (long)	$m/sec$	6000	12890	16400	14920	5460
Specific heat	$J/g^{\circ}K$	3.6	1.82	1.47	0.95	0.134
Heat conductivity	$W/cm^{\circ}C$	0.848	2	7.4	0.3-0.4	1.67
Thermal expansion	$1/^{\circ}C$	$4.6 \times 10^{-6}$	$11 \times 10^{-6}$	$2.7 \times 10^{-6}$	$5 \times 10^{-6}$	$4.3 \times 10^{-6}$

<sup>1</sup> Total mass of Lithium in ~70kg human body is ~7mg.

Heat capacity, Heat conductivity – functions of temperature; this need to be taken into account

## Beam pattern



## Equation for thermal diffusion

$$\nabla(k\nabla T) + \dot{Q} = \rho c_V \dot{T}$$

defines time of relaxation from its characteristic

$$\frac{dx^2}{k} = \frac{dt}{\rho c_V} \rightarrow \delta^2 = \frac{k}{\rho c_V} \tau \rightarrow \tau = \frac{\rho c_V}{k} \delta^2$$

For Be:  $k=2 \text{ W/cm}^\circ\text{K}$ ,  $\rho=1.84\text{g/cm}^3$ ,  $c_V=1.82 \text{ J/g}^\circ\text{K}$

If  $\delta=0.05\text{cm}$

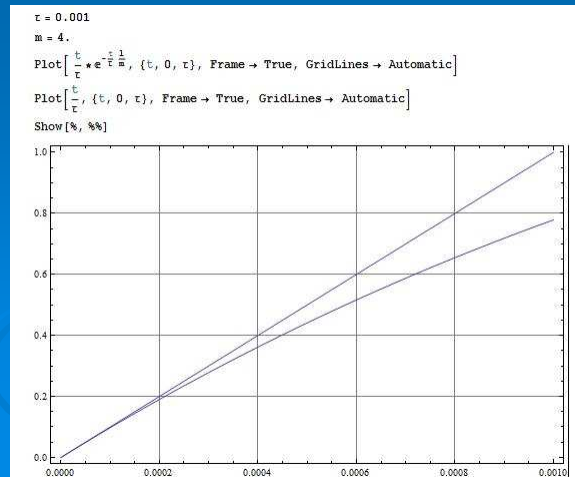
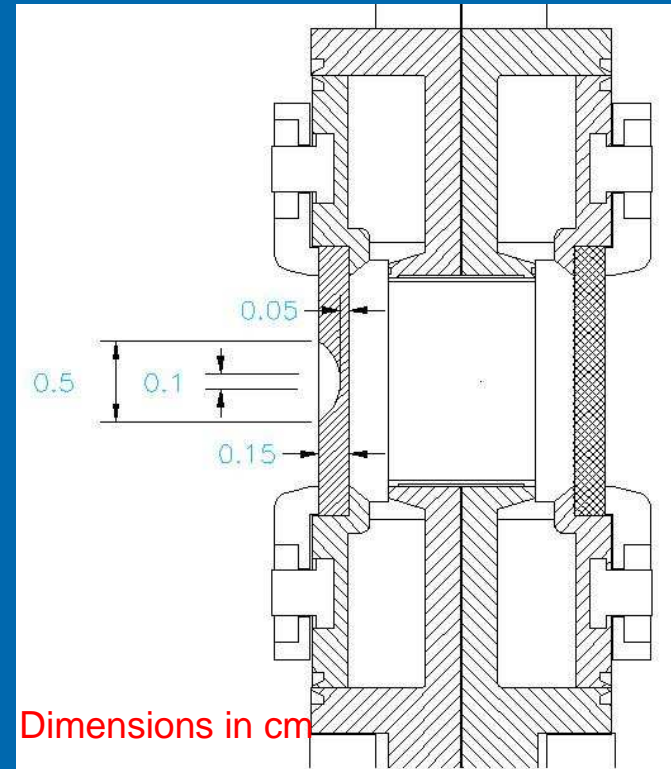
$$\tau = \frac{1.84 \cdot 1.82}{2} 2.5 \cdot 10^{-3} \cong 4.2\text{ms}$$

This gives ~20% temperature drop within train for Be

For Li thermal skin-layer for 1 msec time goes to

$$\delta = \sqrt{\frac{k}{\rho c_V} \tau} = \sqrt{\frac{0.848}{0.533 \times 3.6} 0.001} = 0.021\text{cm}$$

## Flange with recession has faster relaxation time



## LOSSES FOR DIFFERENT MATERIAL OF TARGET

If energy  $Q$  deposited in mass  $m$ , then the temperature rise is

$$\Delta T = \frac{Q}{mc_V},$$

where  $c_V$  stands for the heat capacity. In its turn, for the  $1\text{ cm}^2$  cross section

$$Q \cong l[\text{cm}] \times 1[\text{cm}^2] \times 2[\text{MeV} / \text{g} / \text{cm}^2] \times \rho[\text{g} / \text{cm}^3].$$

For the gamma target, the length  $l$  is a fraction of radiation length,  $l \cong \frac{1}{2} X_0 / \rho$ ,

$$Q \cong X_0 \times 1[\text{MeV}]$$

From the other hand  $m = \rho \times 1[\text{cm}^2] \times \frac{X_0}{2\rho} = \frac{1}{2} X_0 \times 1[\text{g}]$ ,

so the temperature gain goes to be

$$\Delta T \cong \frac{2}{c_V[\text{J} / \text{g} / ^\circ\text{K}]} [^\circ\text{K}] \left( \cong \frac{2A}{25[\text{Mol} / \text{g} / ^\circ\text{K}]} \cong \text{const} : (D - P \text{ law}) \right)$$

For Ti  $c_V=0.5 \text{ J/g} / ^\circ\text{K}$ ; for W  $c_V=0.134 \text{ J/g} / ^\circ\text{K}$ ; for Pb  $c_V=0.13 \text{ J/g} / ^\circ\text{K}$ ,

So ratio of temperatures comes to

$$\Delta T_{Ti} : \Delta T_W : \Delta T_{Pb} \cong 1 : 3.7 : 3.8; \quad (A_{Ti} : A_W : A_{Pb} \cong 47 : 183 : 207)$$

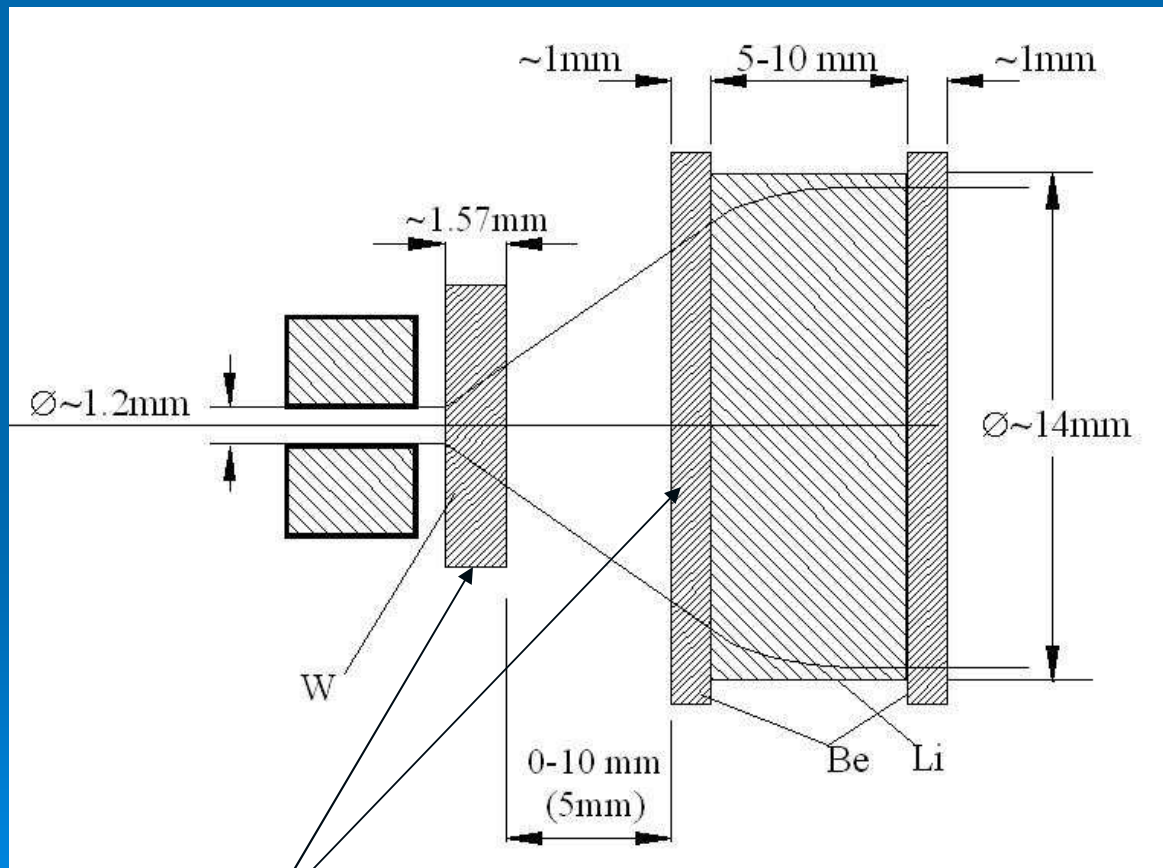
The ratio difference in temperature gain is not so drastic; however it is important if the temperature approaching the melting threshold.

Usage of heavier targets desirable from the point of lowering of focal depth (~10 times) needed to be serviced by capturing optics, however. Also, the positron production efficiency is higher for heavier materials. All together this gives ~50% higher yield for W compared with Ti.

KONN –Monte-Carlo code for positron production starting from undulator

KONN can calculate now the energy deposition and temperature rise in target and in Li lens at any point.

Distance between target and lens serves for enlargement the spot size on the entrance window



← Typical parameters

Target could be combined with entrance flange



## Losses calculated with KONN compared with systematic calculations done with GEANT 3.21 by A.Dubrovin

M.Dubrovin, "Energy Deposition in the Li Lens", Note on Nov 18, 2007, 17pp.

**GOOD AGREEMENT**

## Also with calculations with FLUKA:

S.Riemann, A.Schälicke, A.Ushakov, D.Andrienko, "Activation and Capture simulation", ILC Positron Source Collaboration Meeting", October 29, 2008, 16 pp.

### Deposited Energy per Photon

Part	E [keV/ph]
Target	803.2
Be window (left)	11.6
Li	37.9
Be window (right)	6.5

$$\langle E_{ph} \rangle = 10.4 \text{ MeV}$$

Undulator Length = 131.6 m

Our numbers:  $N_{\gamma\text{tot}} = 101$

1.55 MeV/e (W)

1.44 MeV/e

1.61 MeV/e

1.05 MeV/e

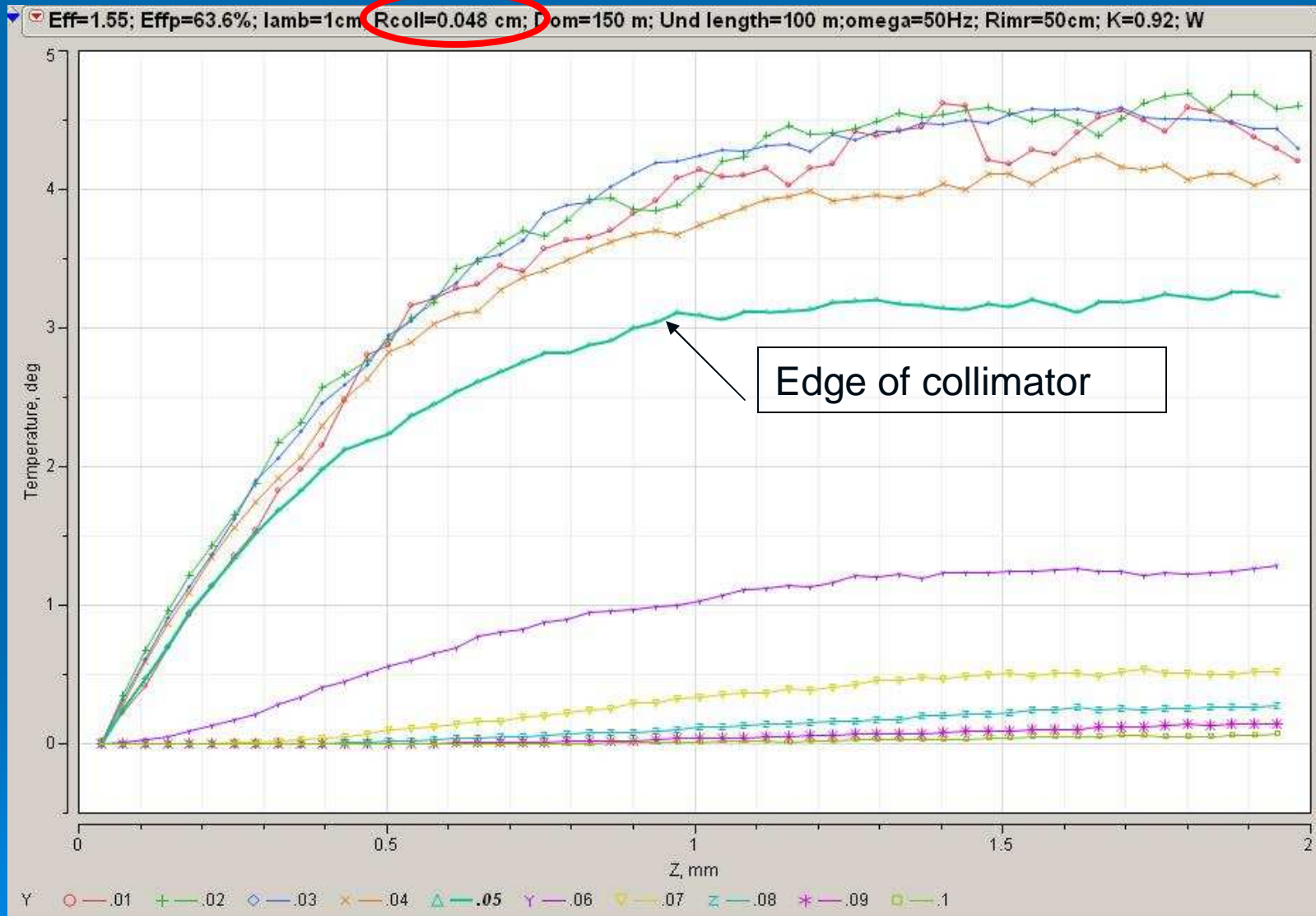
## Also considering calculations with GEANT4:

W.Liu, W.Gai, "Update on Be Window Thermal Issues", HEP, ANL, May 16, 2007

In this publication the gamma beam only was considered; no cooling; Be survives ~20sec

# TEMPERATURE ALONG THE W TARGET FOR DIFFERENT RADIUSSES

per  $10^{13}$  initial electrons



Each particle radiates 2.76 GeV in undulator

Rim W target;

R=50 cm

f=50 Hz

K=0.92

Eff=1.6

Effp=32%

Lund=35m

$\lambda_u=1.15\text{cm}$

Dis=300 m

G=45kG/cm

I=110kA

Rcoll=0.5cm

DISTRIBUTION OF TEMPERATURE IN TARGET T(R,Z) DEG PER 10<sup>13</sup> INITIAL ELECTRONS

DELTA R = .100 cm, DELTA Z = .003 cm

Collimator

R→	0.008	0.005	0.002	0.001	0.000	0.000	0.000	0.000	0.000	0.000
	.300	.113	.030	.004	.000	.000	.000	.000	.000	.000
	.581	.219	.051	.008	.000	.000	.000	.000	.000	.000
	.840	.317	.068	.011	.001	.000	.000	.000	.000	.000
	1.106	.416	.083	.010	.001	.000	.000	.000	.000	.000
	1.408	.504	.097	.011	.001	.000	.000	.000	.000	.000
	1.654	.579	.113	.013	.001	.000	.000	.000	.000	.000
	1.858	.662	.122	.013	.001	.000	.000	.000	.000	.000
	2.060	.749	.135	.014	.001	.000	.000	.000	.000	.000
	2.276	.816	.143	.013	.002	.000	.000	.000	.000	.000
	2.432	.886	.156	.014	.002	.000	.000	.000	.000	.000
	2.616	.946	.158	.015	.002	.000	.000	.000	.000	.000
	2.797	.997	.165	.015	.001	.000	.000	.000	.000	.000
	2.874	1.051	.175	.016	.001	.000	.000	.000	.000	.000
	3.001	1.118	.181	.016	.001	.000	.000	.000	.000	.000
	3.053	1.167	.188	.018	.001	.000	.000	.000	.000	.000
	3.240	1.220	.203	.019	.001	.000	.000	.000	.000	.000
	3.322	1.276	.202	.018	.002	.000	.000	.000	.000	.000
	3.428	1.303	.213	.019	.001	.000	.000	.000	.000	.000
	3.532	1.385	.221	.018	.002	.000	.000	.000	.000	.000
	3.581	1.416	.225	.018	.001	.000	.000	.000	.000	.000
	3.649	1.431	.227	.019	.001	.000	.000	.000	.000	.000
	3.732	1.483	.232	.018	.002	.000	.000	.000	.000	.000
	3.807	1.479	.239	.019	.001	.000	.000	.000	.000	.000
	3.788	1.511	.249	.022	.000	.000	.000	.000	.000	.000
	3.845	1.534	.246	.021	.002	.000	.000	.000	.000	.000
	3.901	1.562	.248	.020	.002	.000	.000	.000	.000	.000
	3.984	1.590	.253	.021	.001	.000	.000	.000	.000	.000
	3.966	1.643	.254	.020	.001	.000	.000	.000	.000	.000
	4.029	1.636	.257	.019	.002	.000	.000	.000	.000	.000
	4.089	1.699	.260	.019	.001	.000	.000	.000	.000	.000
	4.131	1.712	.266	.021	.001	.000	.000	.000	.000	.000
	4.220	1.738	.257	.021	.001	.000	.000	.000	.000	.000
	4.261	1.731	.268	.021	.001	.000	.000	.000	.000	.000
	4.267	1.743	.268	.021	.001	.000	.000	.000	.000	.000
	4.219	1.748	.270	.020	.001	.000	.000	.000	.000	.000
	4.278	1.750	.270	.024	.001	.000	.000	.000	.000	.000
	4.308	1.769	.274	.022	.001	.000	.000	.000	.000	.000
	4.334	1.773	.279	.021	.001	.000	.000	.000	.000	.000
	4.315	1.808	.274	.024	.001	.000	.000	.000	.000	.000
	4.342	1.824	.275	.025	.001	.000	.000	.000	.000	.000
	4.307	1.830	.282	.024	.001	.000	.000	.000	.000	.000
	4.440	1.850	.277	.025	.001	.000	.000	.000	.000	.000
	4.406	1.847	.281	.024	.001	.000	.000	.000	.000	.000
	4.435	1.864	.275	.024	.001	.000	.000	.000	.000	.000
	4.421	1.865	.270	.024	.001	.000	.000	.000	.000	.000
	4.424	1.893	.277	.023	.001	.000	.000	.000	.000	.000
	4.394	1.912	.284	.022	.001	.000	.000	.000	.000	.000
	4.452	1.929	.276	.023	.001	.000	.000	.000	.000	.000

# Now the target is not spinning

DISTRIBUTION OF TEMPERATURE IN TARGET T(R,Z) DEG PER 10<sup>13</sup> INITIAL ELECTRONS

DELTA R = .100 cm, DELTA Z = .003 cm

Collimator

R→										
.178	.111	.052	.012	.001	.001	.000	.000	.000	.000	.000
6.306	2.380	.628	.076	.004	.001	.000	.000	.000	.000	.000
12.211	4.606	1.062	.160	.009	.002	.000	.000	.000	.000	.000
17.650	6.666	1.420	.233	.020	.001	.002	.000	.000	.000	.000
23.229	8.744	1.735	.215	.022	.001	.001	.000	.000	.000	.000
29.563	10.592	2.031	.237	.023	.000	.000	.000	.000	.000	.000
34.737	12.165	2.363	.272	.025	.001	.000	.000	.000	.000	.000
39.023	13.906	2.565	.268	.026	.001	.000	.000	.000	.000	.000
43.268	15.722	2.833	.297	.025	.000	.000	.000	.000	.000	.000
47.793	17.145	3.002	.270	.032	.000	.000	.000	.000	.000	.000
51.077	18.602	3.274	.302	.033	.000	.000	.000	.000	.000	.000
54.937	19.866	3.320	.311	.042	.000	.000	.000	.000	.000	.000
58.733	20.944	3.455	.312	.028	.000	.000	.000	.000	.000	.000
60.357	22.063	3.681	.329	.025	.000	.000	.000	.000	.000	.000
63.027	23.468	3.808	.333	.029	.000	.000	.000	.000	.000	.000
64.106	24.499	3.939	.378	.030	.000	.000	.000	.000	.000	.000
68.045	25.610	4.259	.396	.025	.001	.000	.000	.000	.000	.000
69.764	26.800	4.235	.379	.032	.000	.000	.000	.000	.000	.000
71.979	27.366	4.476	.399	.026	.000	.000	.000	.000	.000	.000
74.173	29.083	4.638	.378	.038	.000	.000	.000	.000	.000	.000
75.208	29.744	4.727	.378	.022	.001	.000	.000	.000	.000	.000
76.633	30.043	4.762	.397	.030	.000	.000	.000	.000	.000	.000
78.364	31.152	4.869	.378	.032	.000	.000	.000	.000	.000	.000
79.947	31.063	5.025	.399	.031	.000	.000	.000	.000	.000	.000
79.545	31.740	5.219	.456	.038	.000	.000	.000	.000	.000	.000
80.736	32.216	5.176	.448	.032	.000	.000	.000	.000	.000	.000
81.911	32.812	5.205	.423	.033	.001	.000	.001	.000	.000	.000
83.666	33.400	5.312	.440	.029	.000	.000	.000	.000	.000	.000
83.296	34.506	5.341	.428	.030	.001	.000	.000	.000	.000	.000
84.613	34.365	5.394	.392	.041	.000	.000	.000	.000	.000	.000
85.876	35.674	5.450	.400	.030	.001	.000	.000	.000	.000	.000
86.751	35.954	5.579	.432	.027	.000	.000	.000	.000	.000	.000
88.622	36.495	5.402	.434	.025	.000	.000	.000	.000	.000	.000
89.485	36.344	5.629	.440	.026	.001	.000	.000	.000	.000	.000
89.609	36.608	5.621	.433	.022	.000	.000	.000	.000	.000	.000
88.595	36.706	5.672	.429	.030	.001	.000	.000	.000	.000	.000
89.832	36.755	5.675	.494	.026	.000	.000	.000	.000	.000	.000
90.468	37.159	5.757	.472	.029	.001	.000	.000	.000	.000	.000
91.011	37.239	5.867	.449	.026	.000	.000	.000	.000	.000	.000
90.623	37.963	5.753	.507	.022	.000	.000	.000	.000	.000	.000
91.176	38.300	5.777	.515	.026	.001	.000	.000	.000	.000	.000
90.441	38.423	5.921	.494	.026	.000	.000	.000	.000	.000	.000
93.246	38.856	5.822	.534	.028	.000	.000	.000	.000	.000	.000
92.526	38.793	5.903	.513	.026	.000	.000	.000	.000	.000	.000
93.128	39.141	5.767	.496	.018	.001	.000	.000	.000	.000	.000
92.849	39.155	5.677	.498	.025	.000	.000	.000	.000	.000	.000
92.913	39.756	5.822	.493	.018	.000	.000	.000	.000	.000	.000
92.267	40.144	5.969	.467	.017	.001	.000	.000	.000	.000	.000
93.494	40.505	5.786	.490	.020	.000	.000	.001	.000	.000	.000



## Temperature in lens

$K=0.92$ ;  $\lambda=1.15$ ;  $Eff=1.6$ ;  $Effp=32\%$ ; Undulator length=35m; Distance to target=300m

DISTRIBUTION OF TEMPERATURE IN LENS T(R,Z) DEG PER  $10^{13}$  INITIAL ELECTRONS

DELTA R = .070 cm, DELTA Z = .050 cm, PHOTONS GENERATED = 76991

	R									
Be entr.	39.396	23.757	16.011	11.015	6.154	3.953	2.325	1.351	.861	.275
	38.128	22.818	15.563	10.848	6.569	4.287	2.792	1.669	1.254	.433
	15.000	9.208	6.263	4.499	2.633	1.745	1.173	.689	.425	.162
	14.017	8.512	6.076	4.383	2.648	1.802	1.217	.795	.492	.197
	13.356	7.904	5.805	4.219	2.664	1.849	1.276	.875	.568	.198
	12.685	7.414	5.488	4.143	2.651	1.842	1.333	.948	.609	.205
Li	12.128	6.922	5.273	4.042	2.591	1.882	1.314	.968	.652	.221
	11.566	6.518	5.049	3.814	2.604	1.856	1.315	.959	.663	.221
	11.103	6.203	4.873	3.616	2.603	1.802	1.297	.904	.709	.213
	10.406	6.081	4.592	3.504	2.588	1.751	1.305	.913	.663	.226
	9.889	5.853	4.370	3.399	2.467	1.774	1.240	.915	.659	.224
	9.733	5.852	4.353	3.523	2.629	1.944	1.376	1.030	.738	.238
	19.89	12.03	9.07	6.89	4.98	3.58	2.46	1.72	1.25	.40
Be exit	20.17	12.17	9.15	6.93	5.04	3.76	2.65	1.84	1.42	.48

# NEW TYPE OF COMMUTATORS FOR HIGH CURRENT



Fig.2. Reverse – switched diodes for peak current from 200 kA to 500 kA and blocking voltage of 2400 V, encapsulated in hermetic metal – ceramic housing and without housing (RSD sizes of 64, 76, and 100 mm)

S.A. Belyaev, V.G.Bezuglov, V.V.Chibirikin, G.D.Chumakov, I.V.Galakhov, S.G.Garanin, S.V.Grigorovich, M.I.Kinzibaev, A.A.Khapugin, E.A.Kopelovich, F.A.Flar, O.V.Frolov, S.L.Logutenko, V.A.Martynenko, V.M.Murugov, V.A.Osin, I.N.Pegoev, V.I.Zolotovskii, "New Generation of High-Power Semiconductor Closing Switches for Pulsed Power Applications", 28 ICPIG, July 15-20, 2007, Prague, Czech Republic, Topic#17, pp.1525-1528.

General parameters	
Energy of primary beam	~150 GeV-350GeV
Undulator period $\lambda$	10-12 mm
$K$ factor, $K = eH\lambda/2\pi/mc^2$	0.4-1
Undulator length	$\leq 200$ m
Efficiency, $e^+ / e^-$	$\geq 1.5$
Polarization	$\geq 65\%$
Target W/Ti	1.75 mm/14.8 mm
Energy of quanta	~9-20 MeV
Distance to the target	100-300 m
Lens	
Feeding current, $I$	<150 kA
Field at surface, $H_m$	43 kG
Gradient	$\leq 62$ kG/cm
Pulsed power	~200kW
Average power	~4kW
Pulsed duty, $\tau$	<4msec
Lens diameter, $2a$	1 cm
Length, $L$	0.5-1 cm**
Axial pressure, $P_0$	74atm (for $L=0.5$ cm)
Temperature gain per train	$\leq 170^\circ\text{C}$ at 150kA

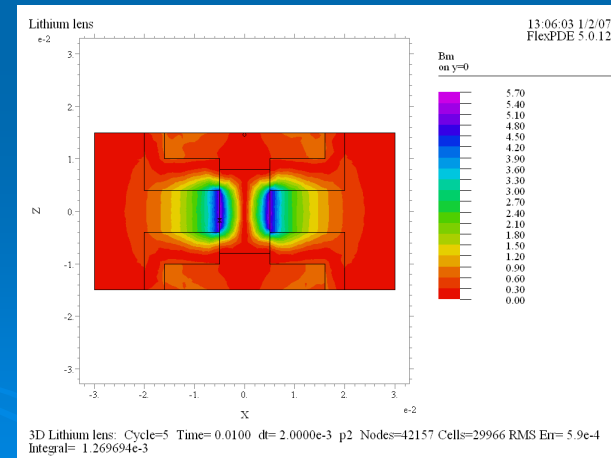
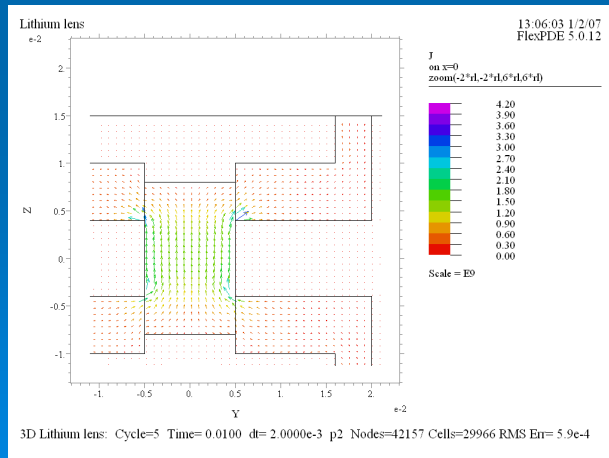
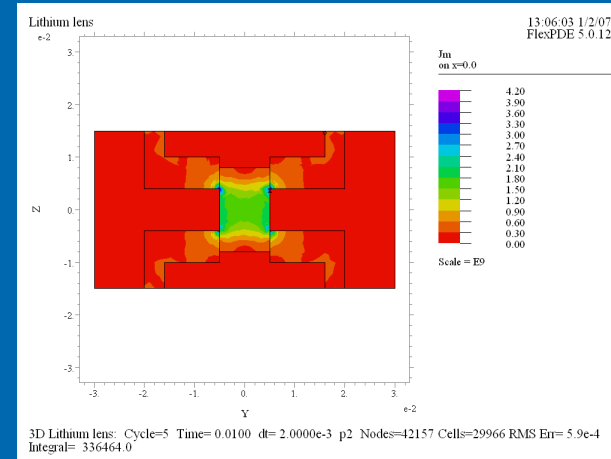
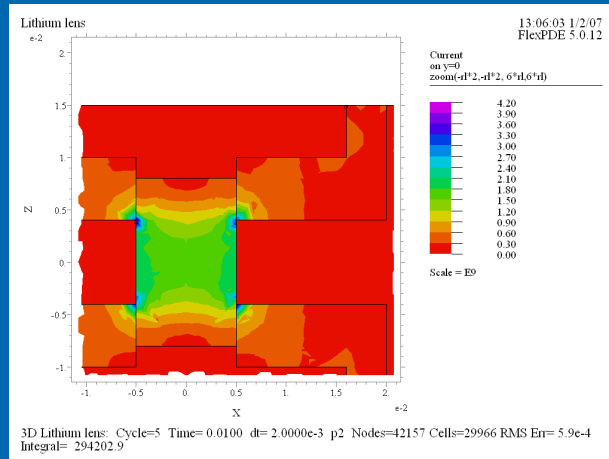


# SUMMARY

- In KONN, to efficiency calculations, added the possibility to calculate losses and temperature gain normalized to initial electron beam population.
- With KONN there were calculated conversion scenarios at 150, 250, 350 GeV with  $K=0.29-0.92$  including thermal effects; at every energy, efficiency  $\geq 1.5$ , Pol  $>65\%$  obtained.
- General conclusion is that spinning Tungsten target survives irradiation in all scenarios including  $K=0.92$  .
- Finished design of Li lens; it allows easy exchange of windows, lens position in housing could be adjusted with respect to the target and acceleration structure .
- Tungsten target could be combined with the entrance window of Lithium lens.
- All necessary preparations done for further modeling of dynamic heating processes such as shock waves, cyclic expansions, Li flow etc.
- New round of optimizations with thermal effects will be done
- Solenoidal lens will be implemented in KONN also

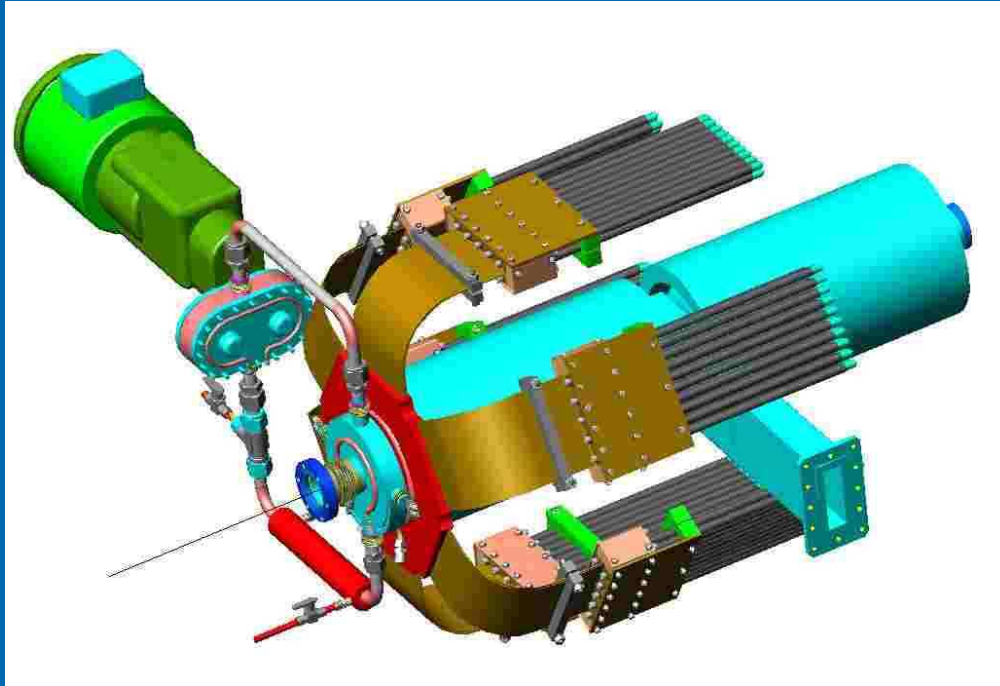
# Backup slides

# Recent calculation of Lithium lens done with FlexPDE<sup>®</sup> code at Cornell



Time dependent 3D calculations

Li lens can be used with any target: liquid metal (Pb-Bi, Hg) or Ti rim



Right after the target located Aluminum made accelerating structure immersed in solenoidal magnetic field.

Sectioned solenoid wound with Al conductor. Sections supplied with reversed polarities